

Attenuation of Waves and Surge by Vegetation

Weiming Wu, PhD
Professor

Dept. of Civil and Environmental Eng.
Clarkson University
Potsdam, NY 13699, USA

Wave Attenuation by Vegetation



- Sponsored by SERRI, DHS
- Lab/Field Experiments & Computational Modeling
- Ole Miss, LSU, NSL



Research Team

- **PI:** Dr. Weiming Wu

Computational modeling team:

- Dr. Weiming Wu, Dr. Yan Ding, Dr. S. N. Kuiry, Dr. Mingliang Zhang, Mr. Reza Marsooli (NCCHE)

Laboratory experiment team:

- Dr. Daniel Wren (NSL), Dr. Yavuz Ozeren (NCCHE)

Field investigation team:

- Dr. Qin Chen, Dr. Guoping Zhang, Mr. Ranjit Jadhav, Mr. James Chatagnier, Kyle Parker, James Bouanchaud, Hem Pant (LSU)
- Dr. Marjorie Holland, Miss Ying Chen (UM-Biology)

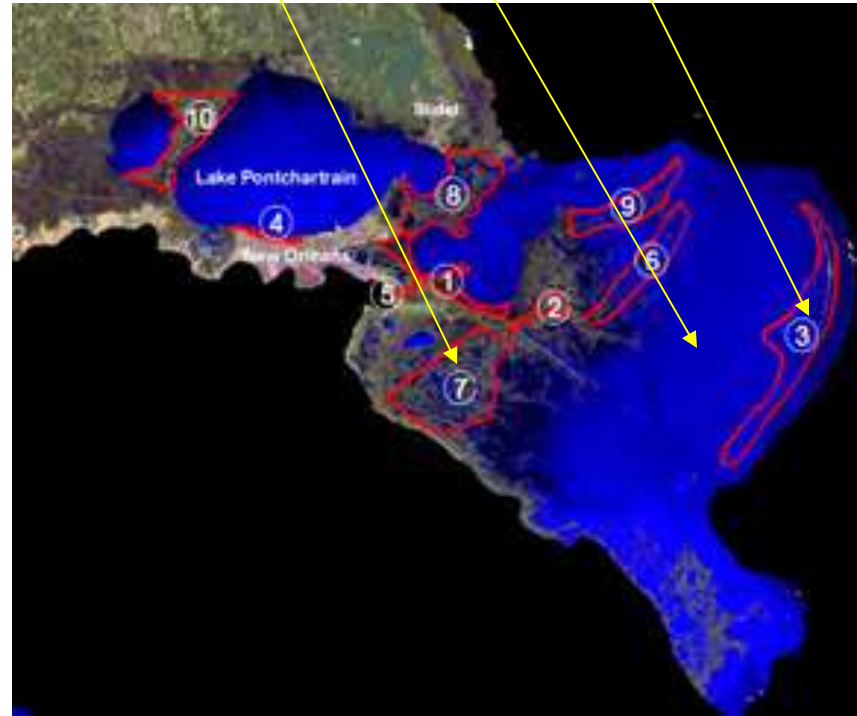
Laboratory and Field Experiments of Wave Attenuation by Vegetation

(Project period: 2009-2012)

Coastal Protection



John Lopez, 2006. Courtesy of Lake Pontchartrain Basin Foundation



- Multiple Lines of Defense

Surge/Wave vs. Vegetation



Vegetation attenuates waves and surge, while it is stressed by waves and surge.

Marsh Edge Erosion by Waves and Surges

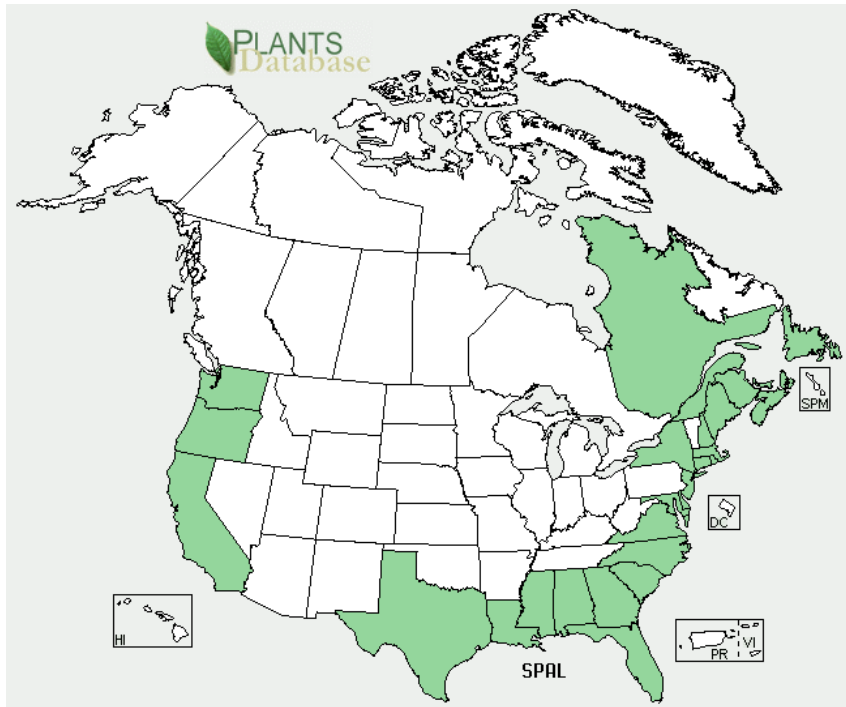
Louisiana has lost 1,829 square miles of land since the 1930's (Barras et al. 2008, Britsch and Dunbar 1993)

Between 1990 and 2001, wetland loss was approximately 13 square miles per year- that is the equivalent of approximately one football field lost every hour (Barras et al. 2008). According to land loss estimates, Hurricanes Katrina and Rita transformed 198 square miles of marsh to open water in coastal Louisiana (Barras et al. 2008).



Studied Vegetation Species I:

Spartina alterniflora Loisel.

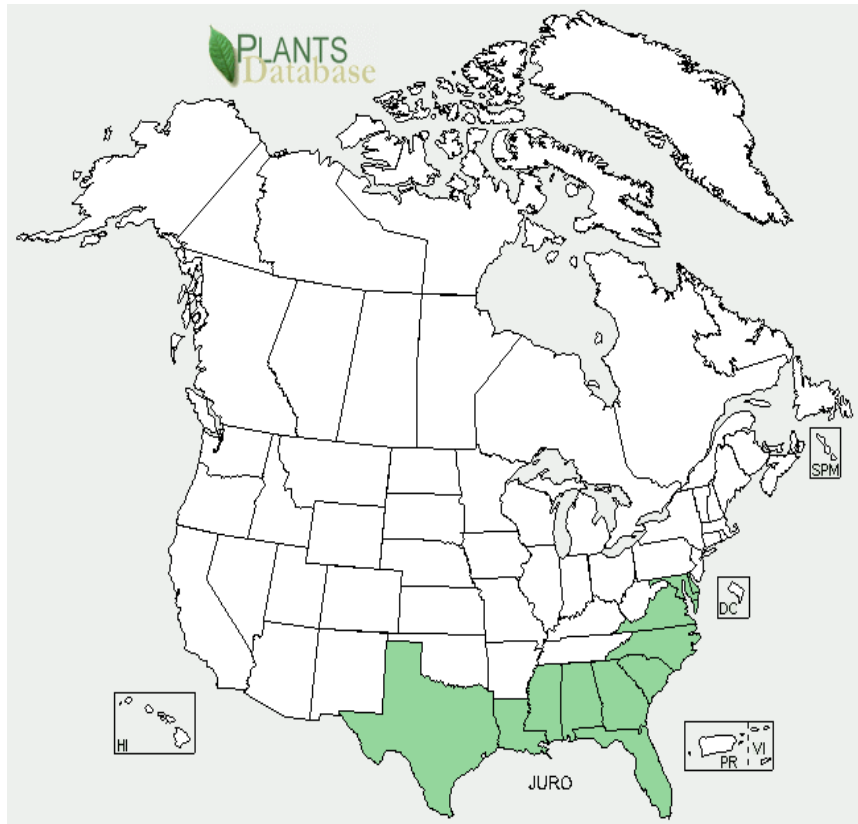


<http://plants.usda.gov/maps/large/SP/SPAL.png>

Spartina alterniflora at Terrebonne Bay, LA (4/4/2011)

Studied Vegetation Species II:

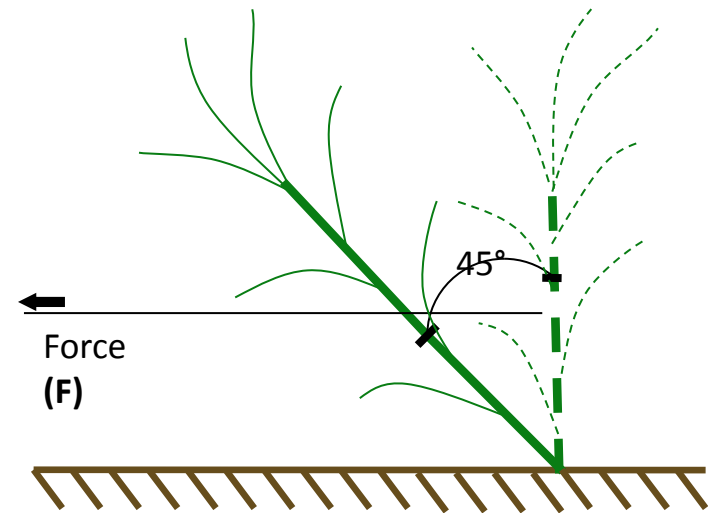
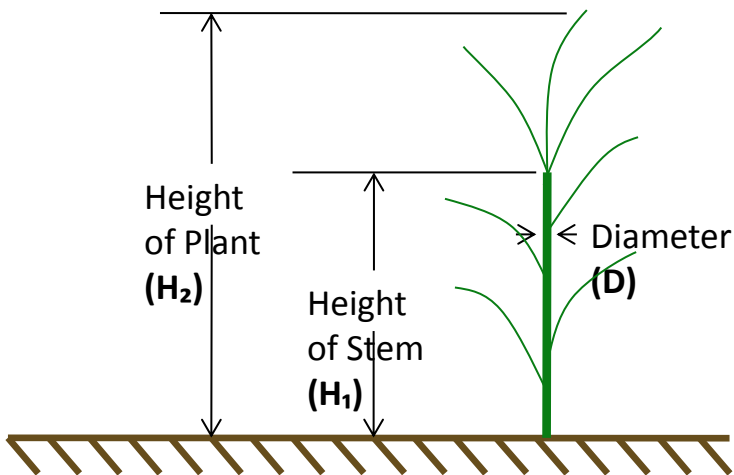
Juncus roemerianus Scheele



<http://plants.usda.gov/core/profile?symbol=JURO>

Smooth Cord Grass Bending Stiffness

- Measurement Procedure:
 - Total plant height and stem height are measured
 - A clip is attached at half the stem height
 - Plants are pulled to a 45° angle
 - Force needed is measured with a force gauge
 - Plant is cut at base and maximum stem diameter is measured

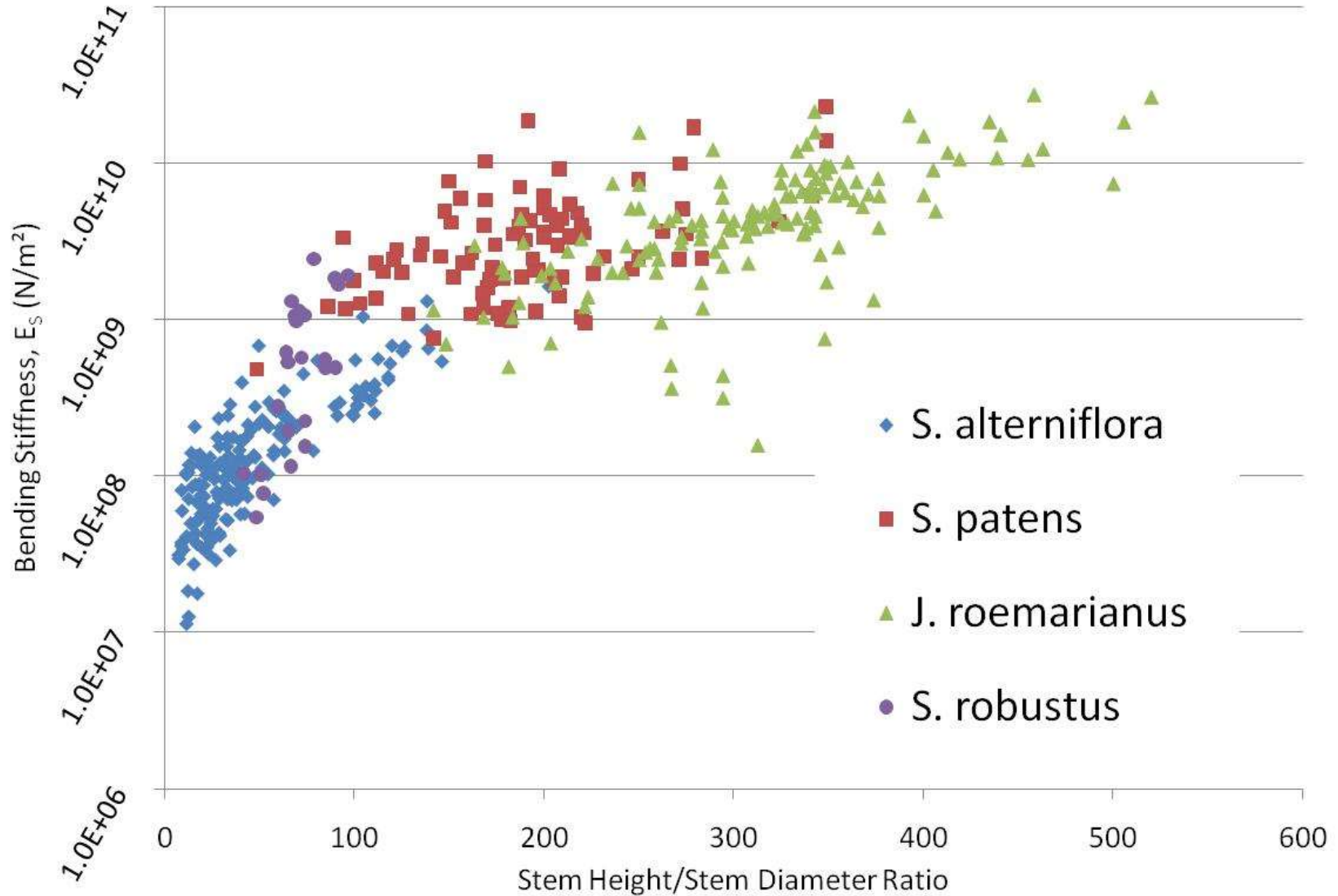


Vegetation Properties



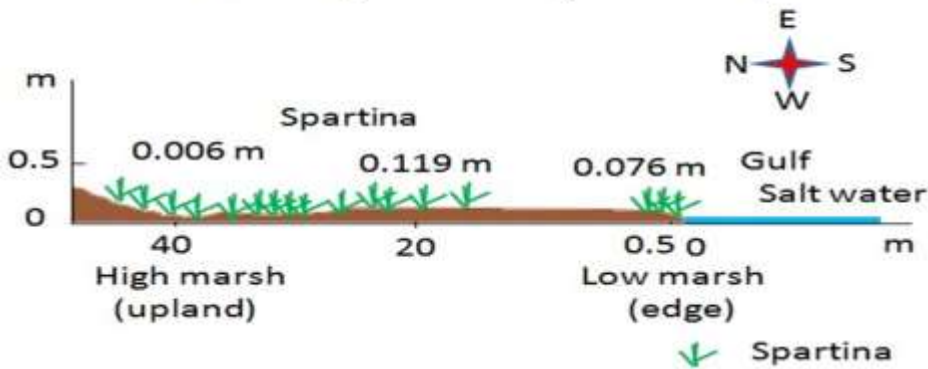
Plant Stiffness Modulus

All Live Plants E_s vs Stem Height/Stem Diameter

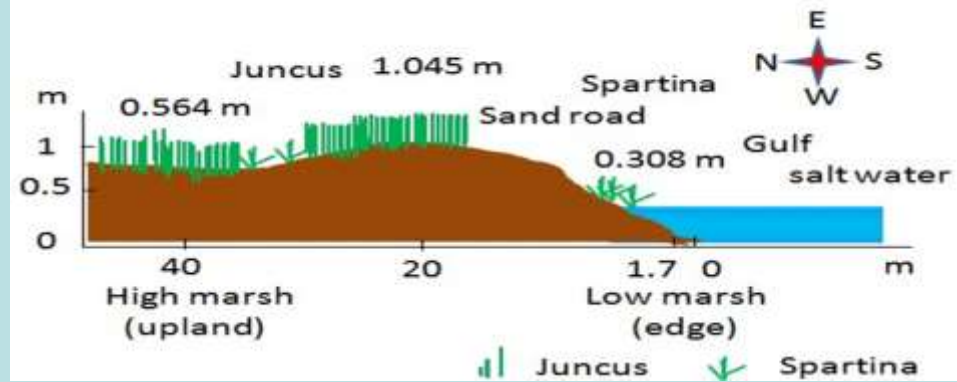


Zonation of eight experimental transects at Grand Bay and Graveline Bayou, MS (four coastal transects)

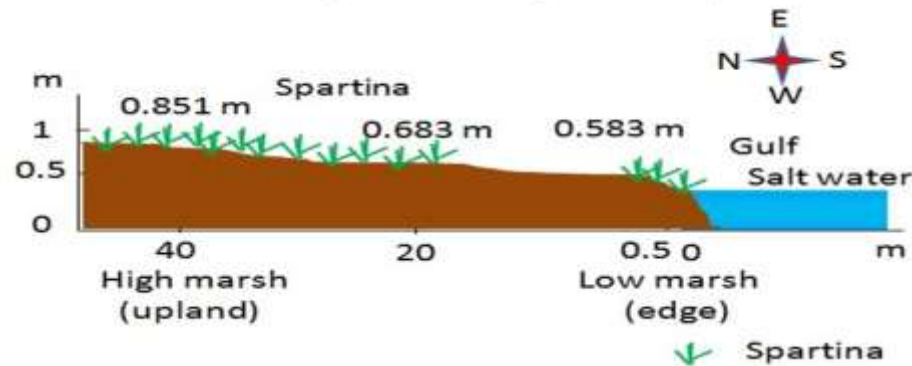
Transect 1 Rigolets Island (West coast)



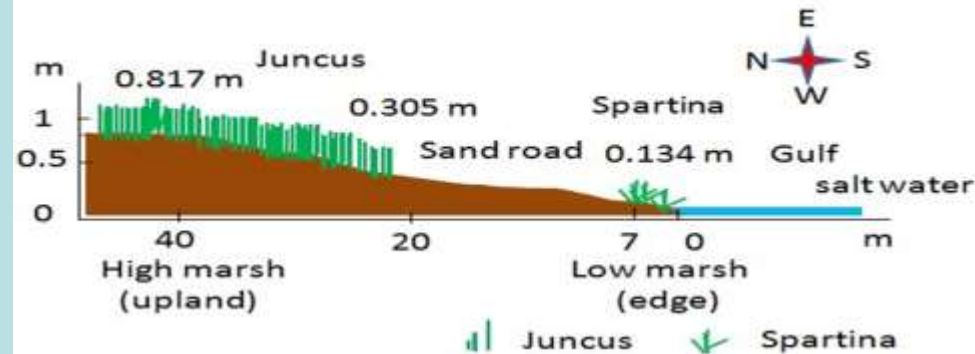
Transect 6. South Graveline Bayou (West coast)



Transect 2. Rigolets Island (East coast)

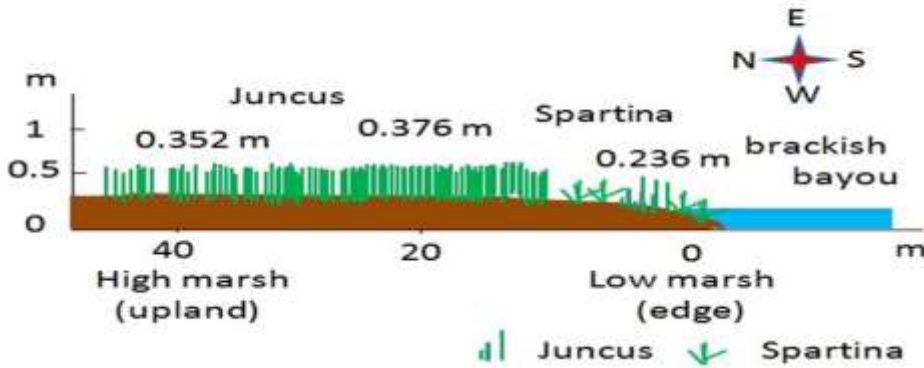


Transect 7. South Graveline Bayou (East coast)

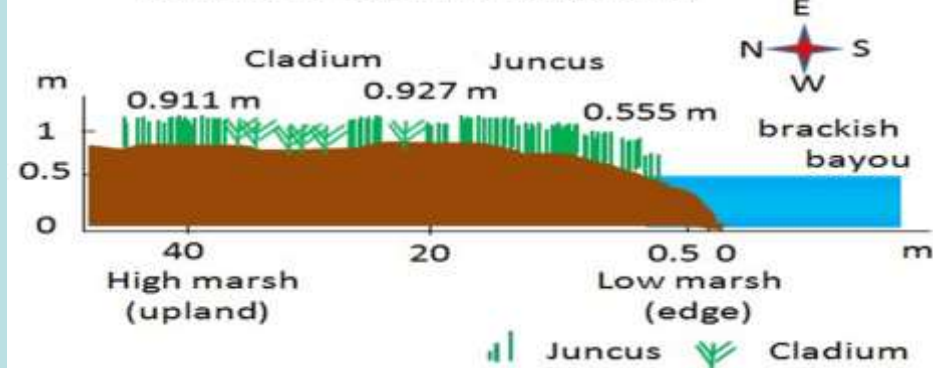


Zonation of eight experimental transects at Grand Bay and Graveline Bayou, MS (four inland transects)

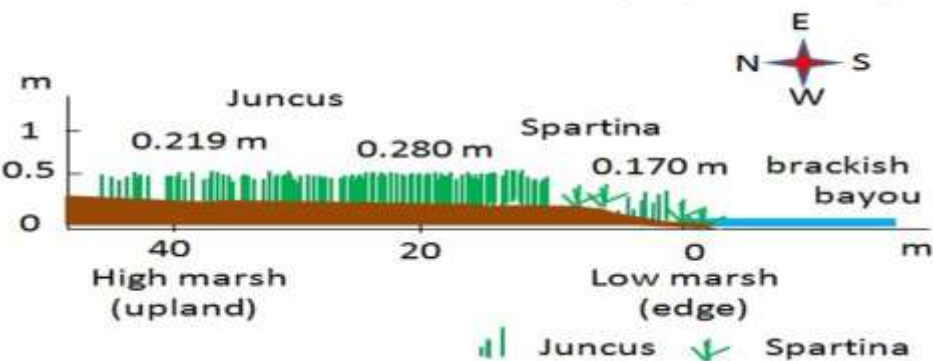
Transect 3. North Graveline Bayou (West inland)



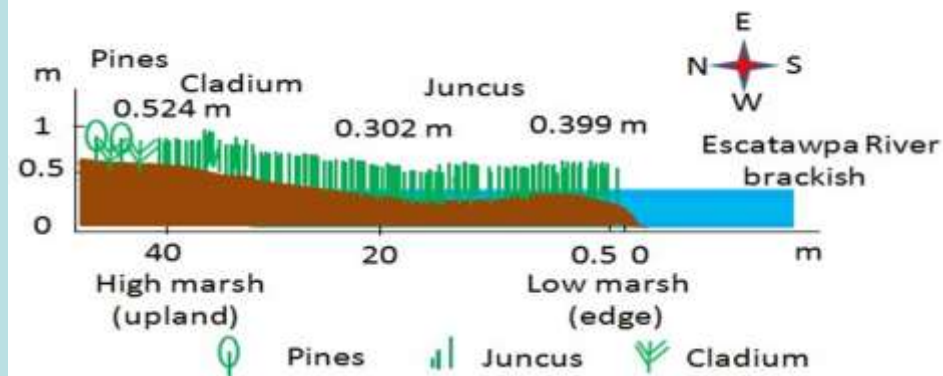
Transect 5. Bayou Heron (inland)



Transect 4. North Graveline Bayou (East inland)



Transect 8. Orange Grove site at Grand Bay (inland)

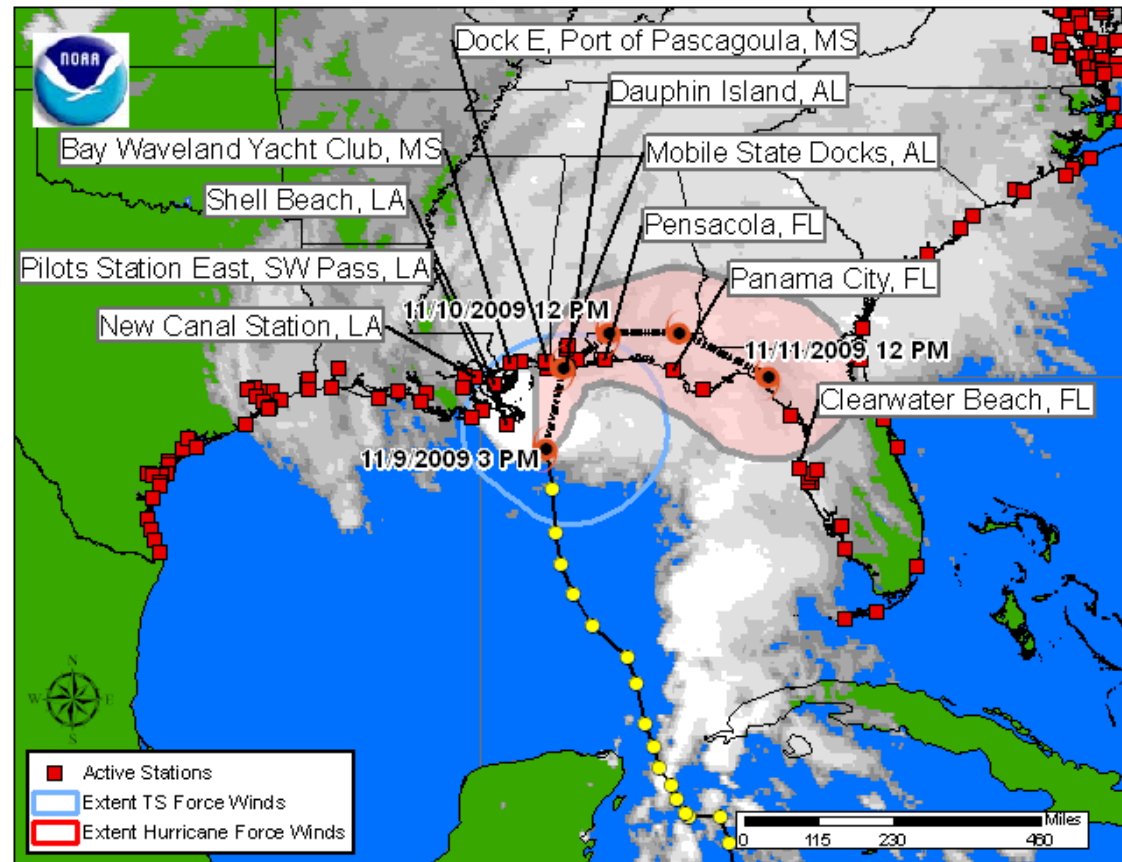


Vegetation characteristics of low and high marsh zones combined in eight transects

Zones	Dominant species	Live standing shoot heights (m)	Dead standing shoot heights (m)	Mean % cover	Rhizome thickness (cm)
Low marsh zone	<i>Spartina alterniflora</i>	0.45-1.40 (0.85)	0.30-0.75 (0.54)	71.41	0.49
	<i>Juncus romerianus</i>	0.78-1.45 (1.17)	0.67-1.52 (1.04)		0.54
High marsh zone	<i>Spartina alterniflora</i>	0.78-2.30 (1.34)	0.83-1.45 (1.11)	80.50	0.54
	<i>Juncus romerianus</i>	1.40-2.30 (1.73)	0.8-1.75 (1.30)		0.58

Short-term Rapid Deployment during Tropical Storm/ Hurricane (Tropical Storm Ida Measurements)

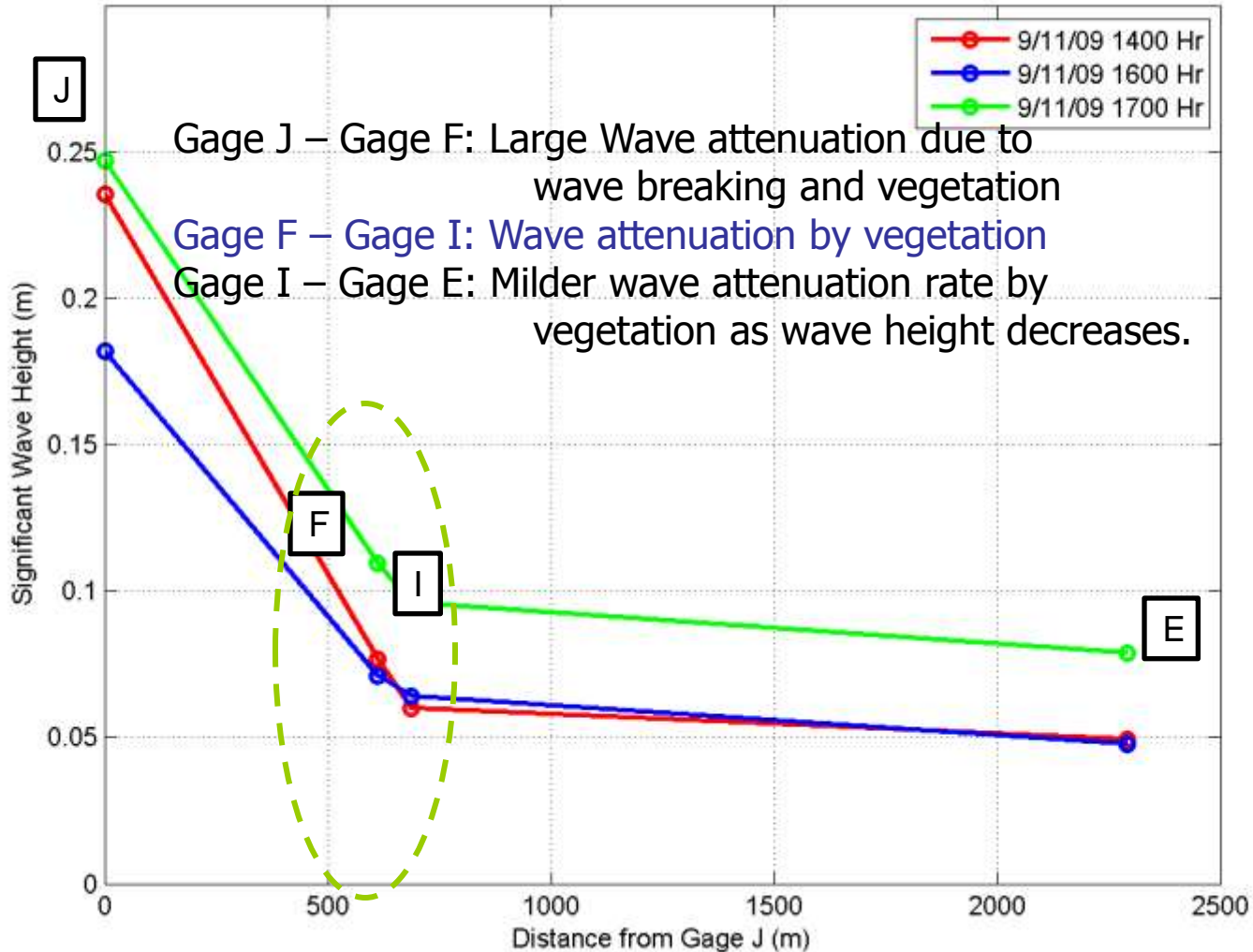
- Landfall on Nov. 10, 2009 on the Mississippi coast
- Five wave gages were deployed by LSU on Nov. 9, 2009 in Breton Sound, LA
- All gages were retrieved after 11 days
- Measured waves and surge analyzed

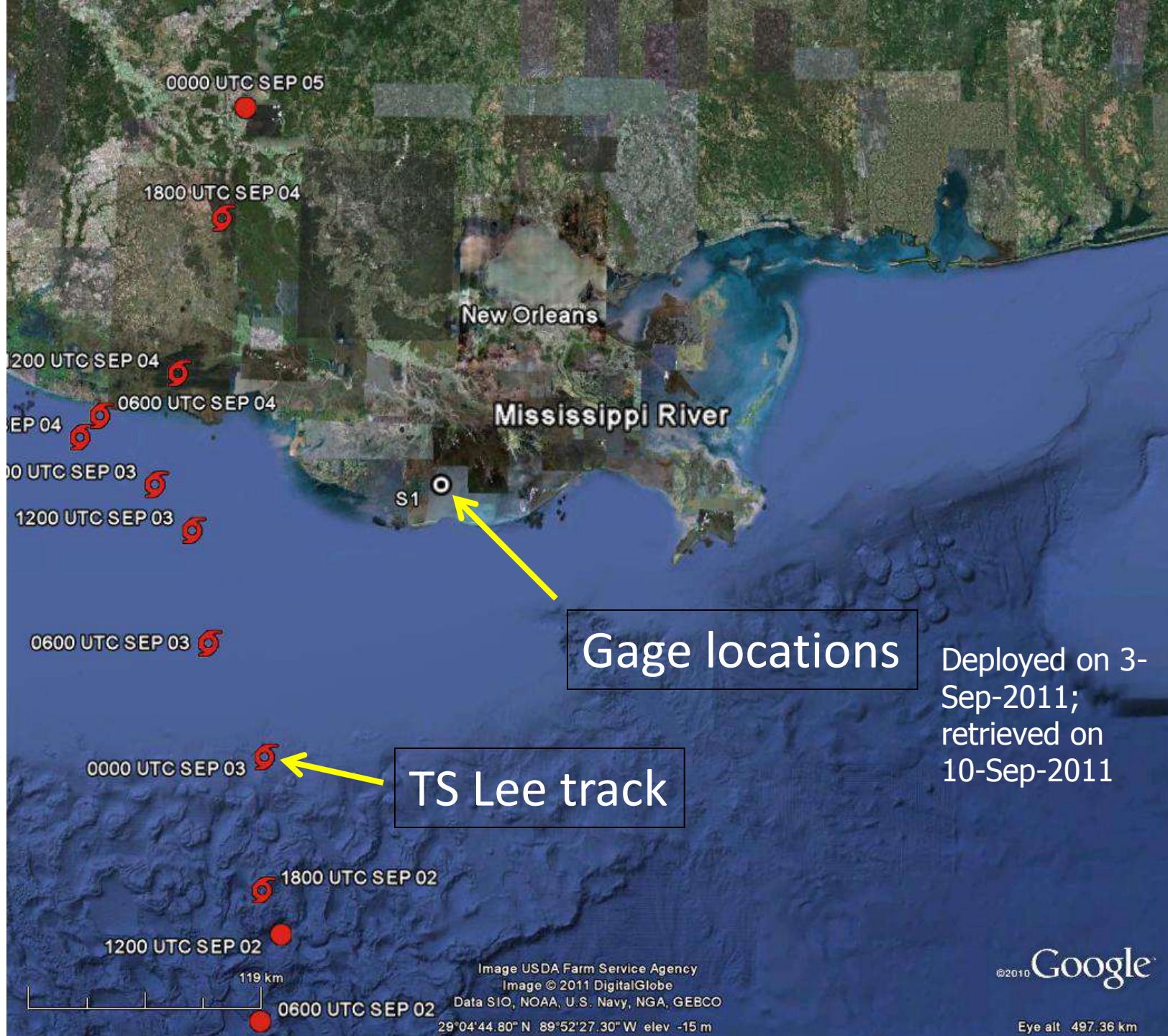


Tropical Storm Ida Deployment –Gage Locations



Tropical Storm Ida: Measured Wave Height Attenuation





0000 UTC SEP 05

1800 UTC SEP 04

New Orleans

Mississippi River

S1

Gage locations

Deployed on 3-Sep-2011;
retrieved on 10-Sep-2011

TS Lee track

0000 UTC SEP 04

0600 UTC SEP 04

SEP 04

0000 UTC SEP 03

1200 UTC SEP 03

0600 UTC SEP 03

0000 UTC SEP 03

1800 UTC SEP 02

1200 UTC SEP 02

0600 UTC SEP 02



Image USDA Farm Service Agency
Image © 2011 DigitalGlobe
Data SIO, NOAA, U.S. Navy, NGA, GEBCO
29°04'44.80" N 89°52'27.30" W elev -15 m

©2010 Google

Eye alt 497.36 km

Surge gages

Wave gages

S6

S5

S4

S3

S2

S1

W0-W4

Image USDA Farm Service Agency
Image © 2011 GeoEye
Image © 2011 DigitalGlobe

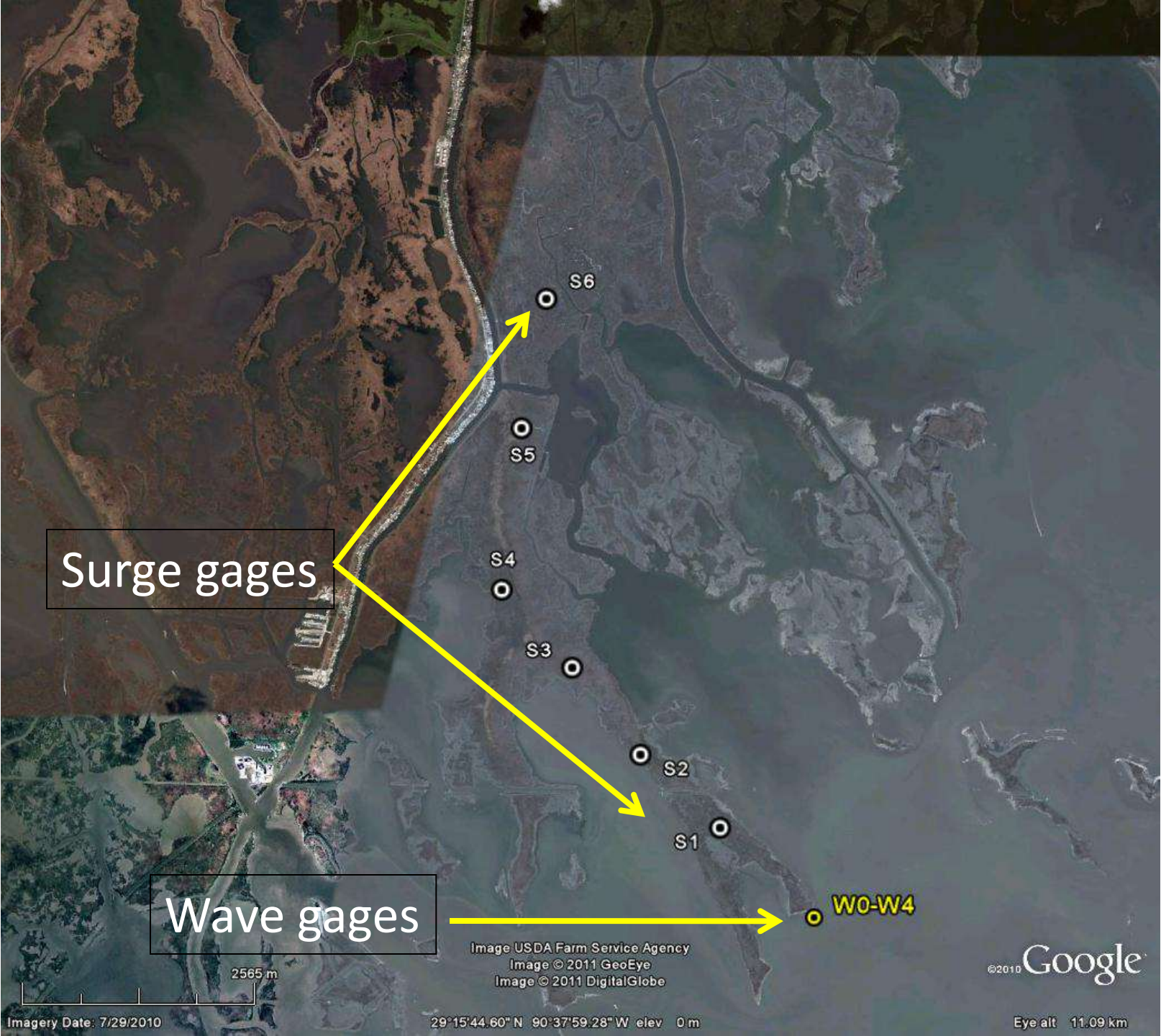
©2010 Google

Imagery Date: 7/29/2010

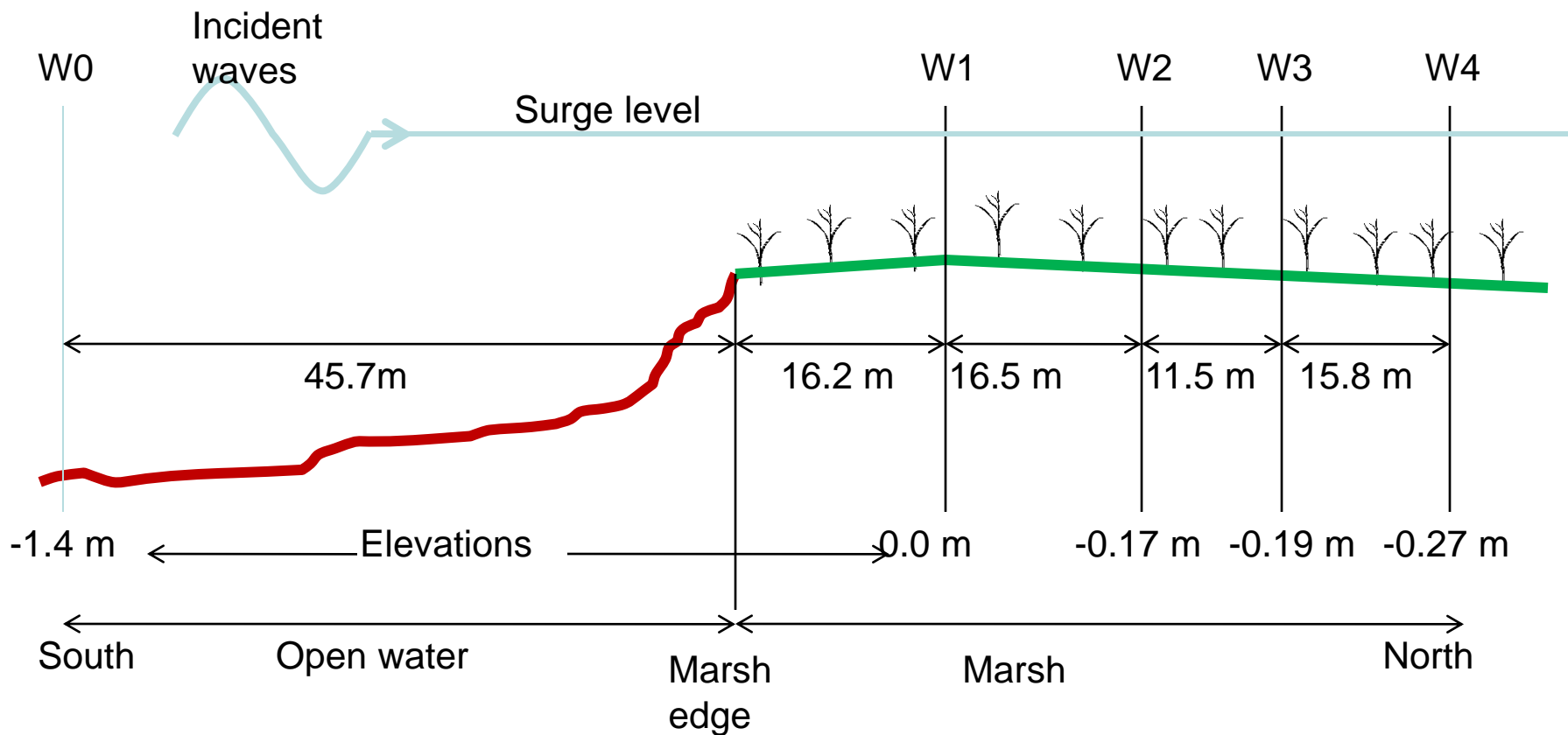
29°15'44.60" N 90°37'59.28" W elev 0 m

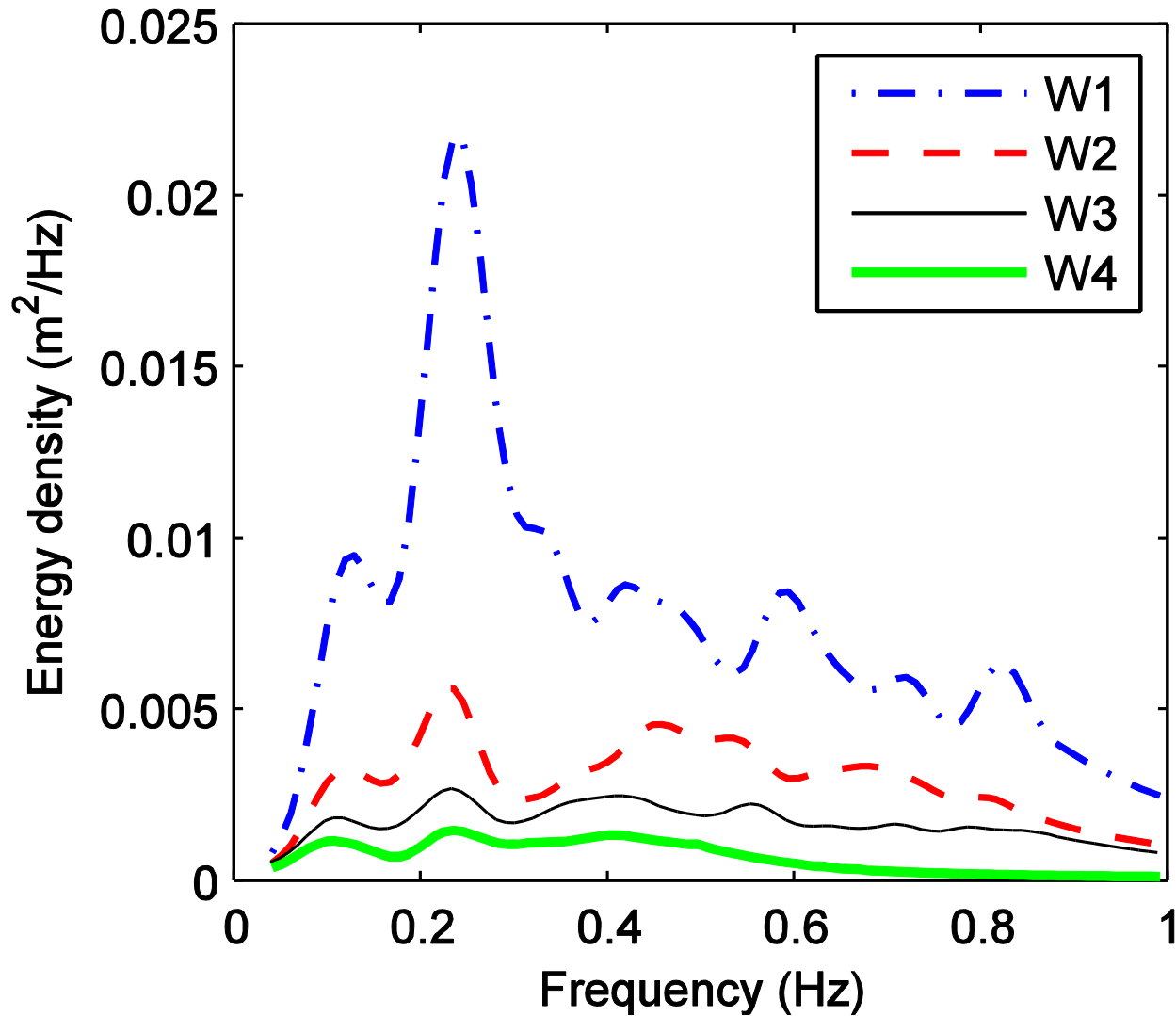
Eye alt 11.09 km

2565 m

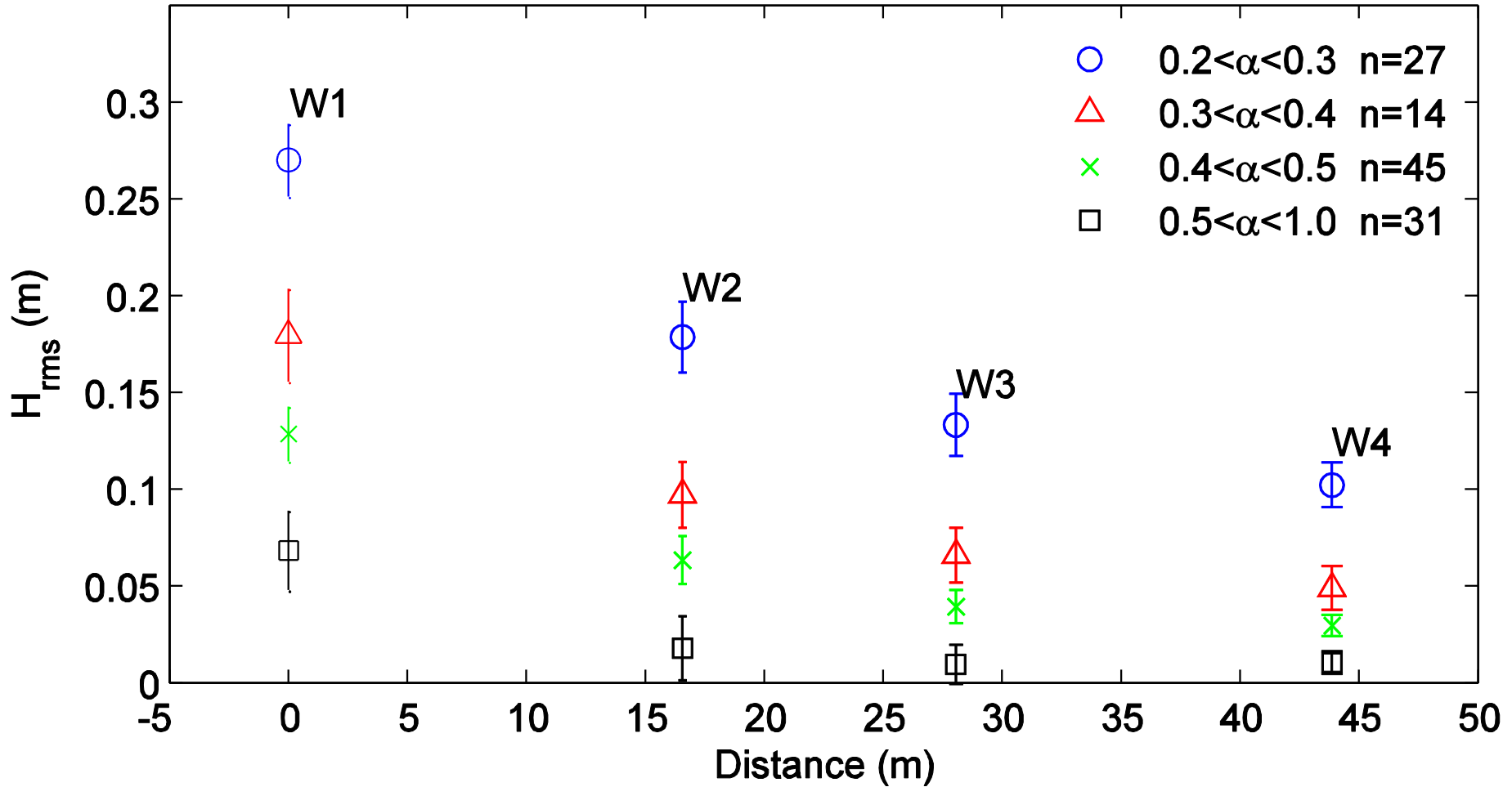


Details of wave gage locations





Sample of simultaneous wave spectra recorded at 4 marsh gages



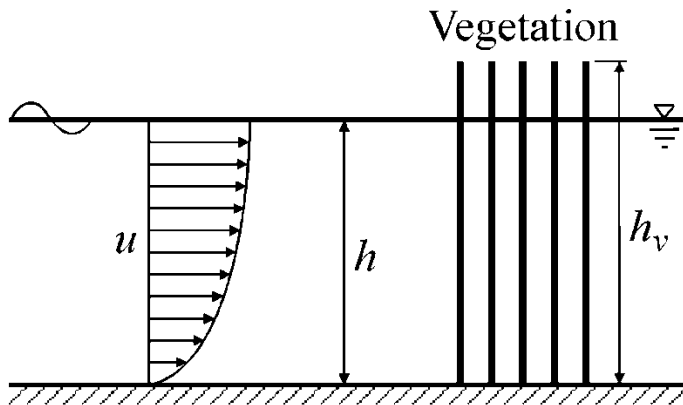
Spatial variation of measured wave heights at four marsh gages for various ranges of submergence ratio, α , at gage W1. Number of records in each range is given by n . Symbols indicate mean values and vertical bars are ± 1 standard deviation. Using α from one gage only for classification ensures that the same waves are followed across the transect to compute the mean.

Drag Force of Vegetation

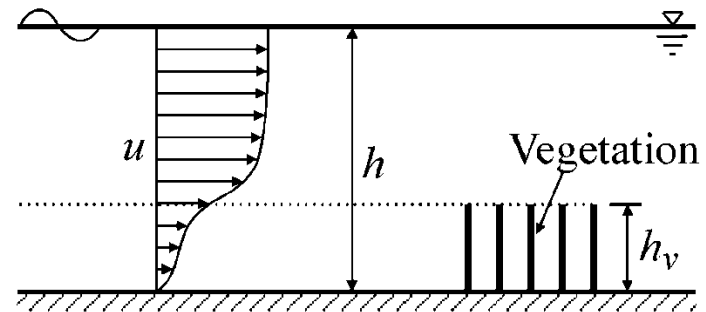
$$\vec{F}_D = \frac{1}{2} C_D \rho N_v A_v |\bar{U}_v| \vec{U}_v$$

For submerged vegetation, Stone and Shen's (2002) method:

$$U_v = \eta_v \left(\frac{h_v}{h} \right)^{0.5} U$$



(a) Emergent



(b) Submerged

Wave Energy Dissipation through Vegetation (Mendez and Losada, 2004)

$$Q_v = \frac{1}{2\sqrt{\pi}} \rho C_D b_v N_v \left(\frac{kg}{2\sigma} \right)^3 \frac{\sinh^3(k\alpha h) + 3 \sinh(k\alpha h)}{3k \cosh^3(kh)} H_{rms}^3$$

Assumptions:

- (1) Linear waves
- (2) Impermeable bottom
- (3) Invariant Rayleigh wave height distribution
- (4) Thornton and Guza's wave breaking criteria

b_v = plant area per unit height of each vegetation stand normal to horizontal velocity (m)

N_v = number of vegetation stands per unit horizontal area (m⁻²)

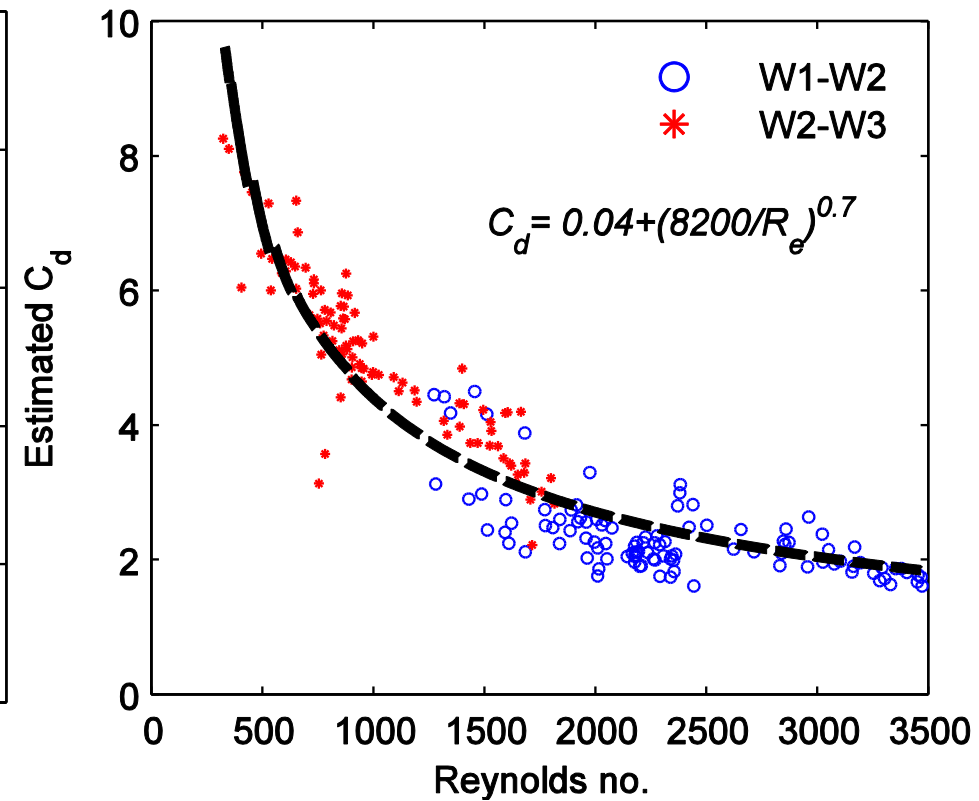
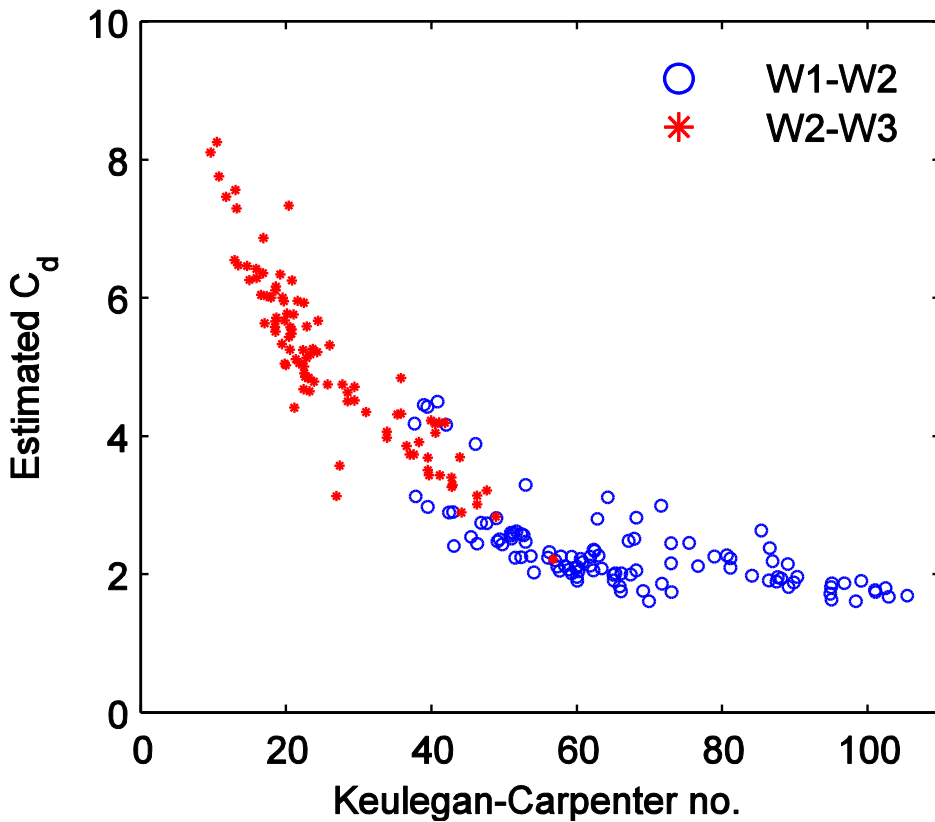
C_D = drag coefficient for irregular waves

H_{rms} = root-mean-square wave height (m)

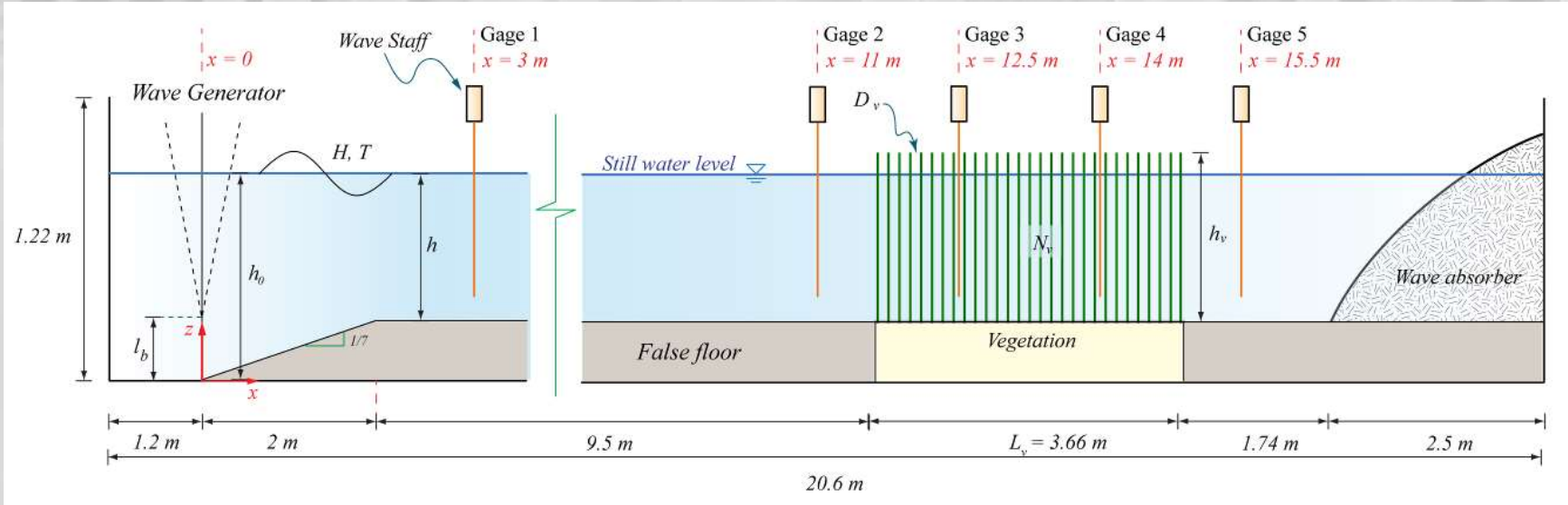


Terrebonne Bay, LA, 5/3/2009

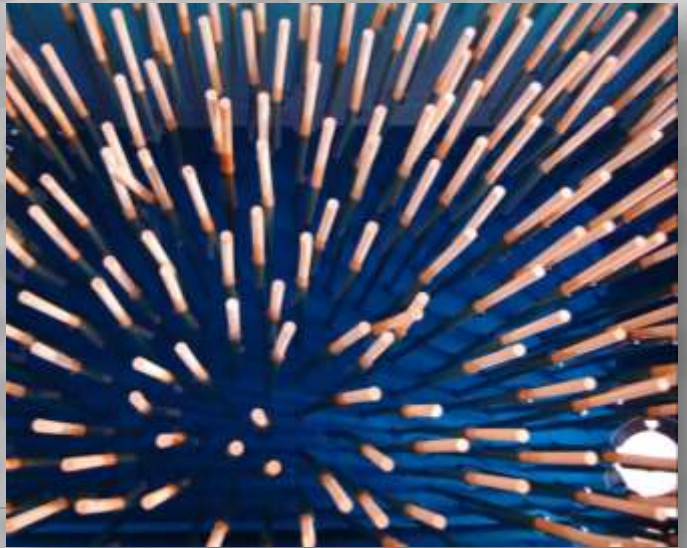
Estimated Vegetation Drag Coefficient C_d using Dalrymple (1984)



Laboratory Experiments



Rigid Vegetation



Live Vegetation



Video

Rigid Model Vegetation

Water depth: 50 cm

Wave height: 10.2 cm

Wave period: 1.2 s

Veg. Density: 623 stems/m²

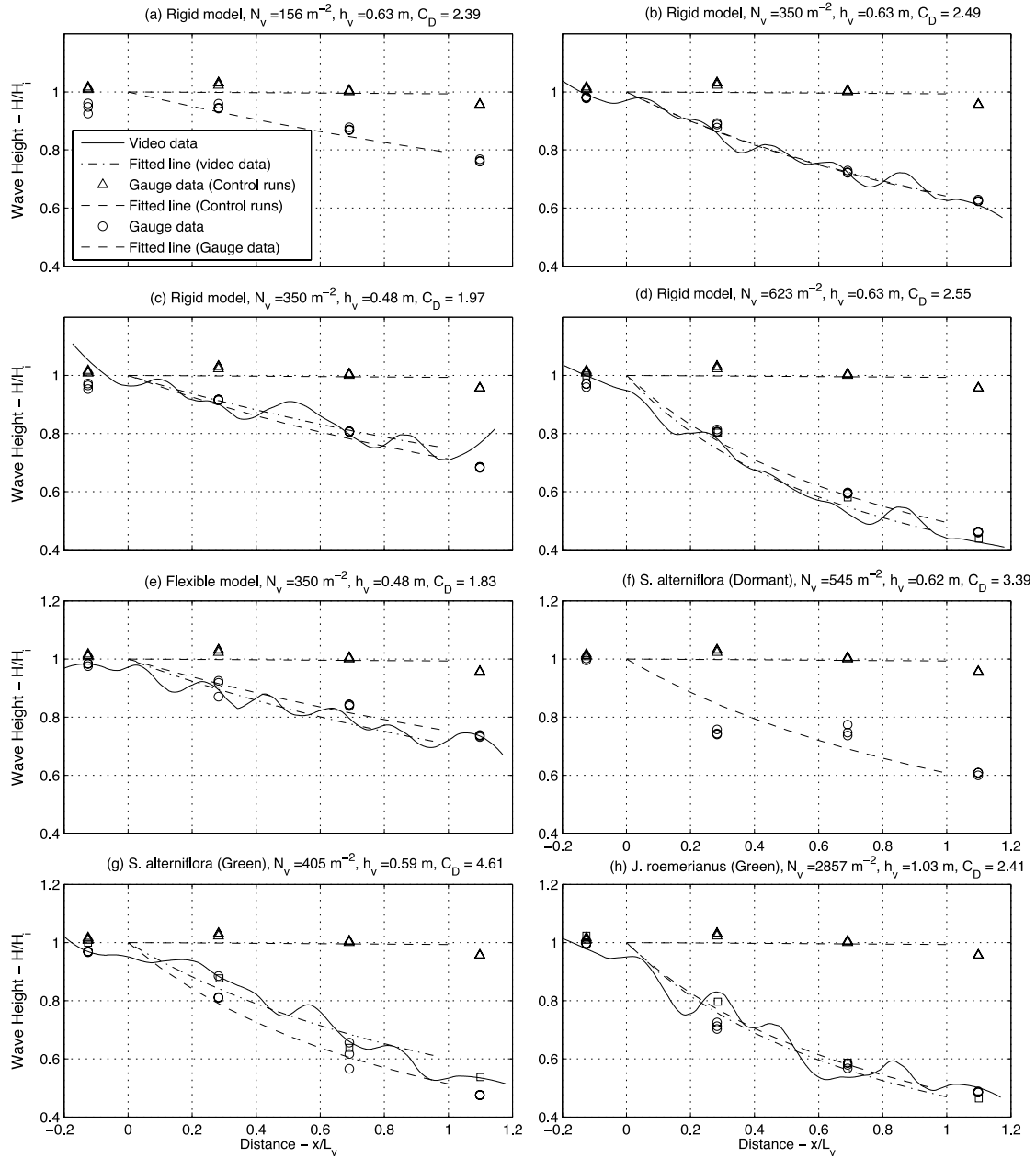
Veg. span: 3.6 m

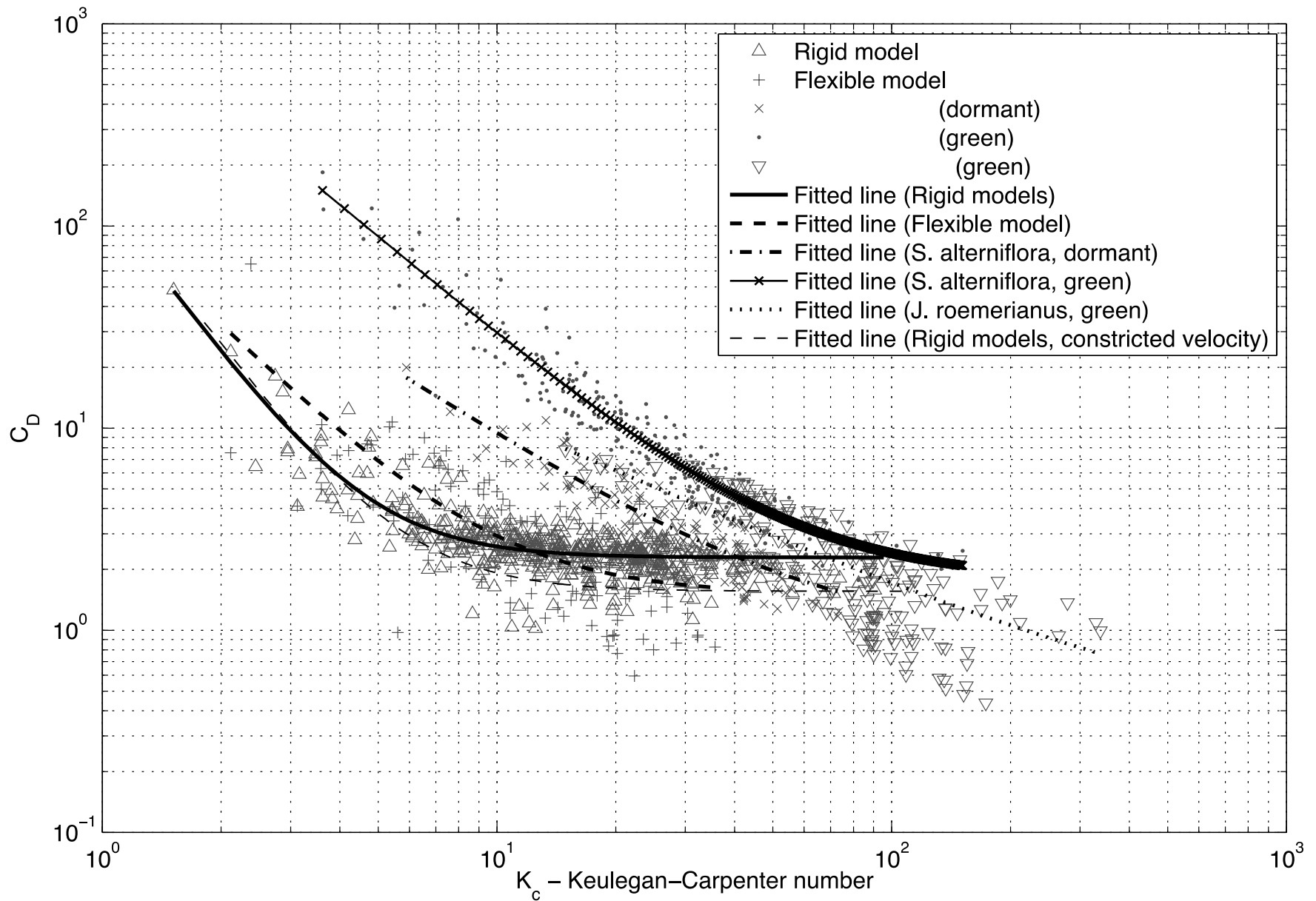
t 00:00:30.0
501021201
12636301

Video (Live Vegetation)

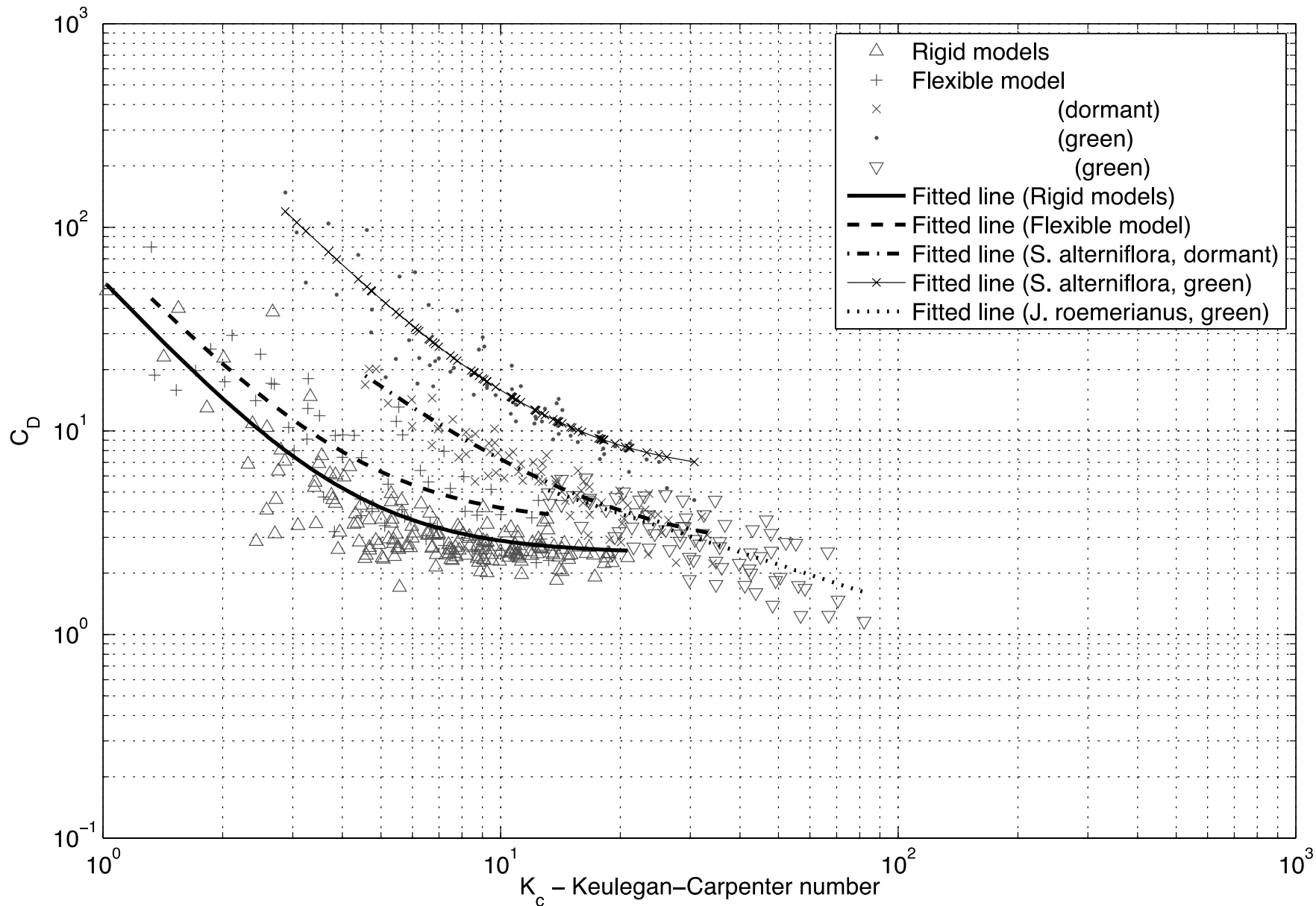


Wave heights affected by different vegetation



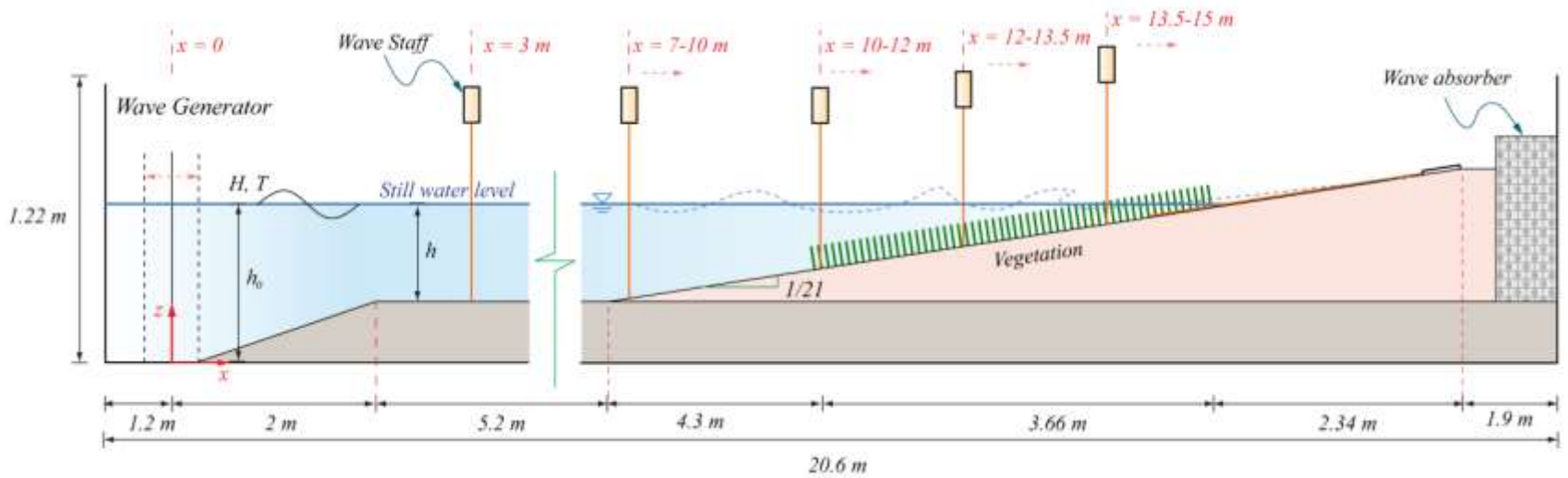


Average trends of the drag coefficient for rigid, flexible and live vegetation models under regular waves.



Average trends of the drag coefficient for rigid, flexible and live vegetation models under random waves.

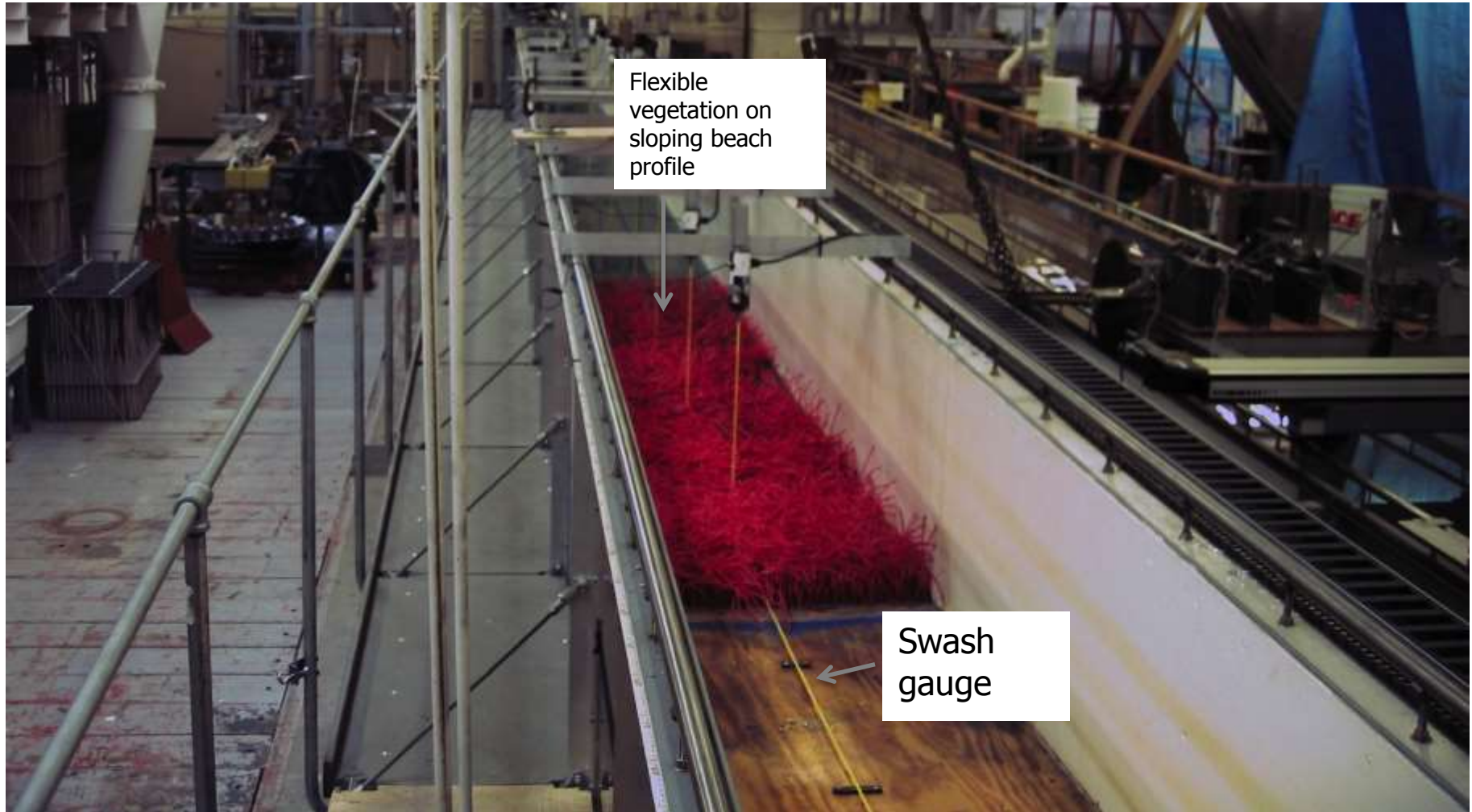
Sloping Beach Experiments



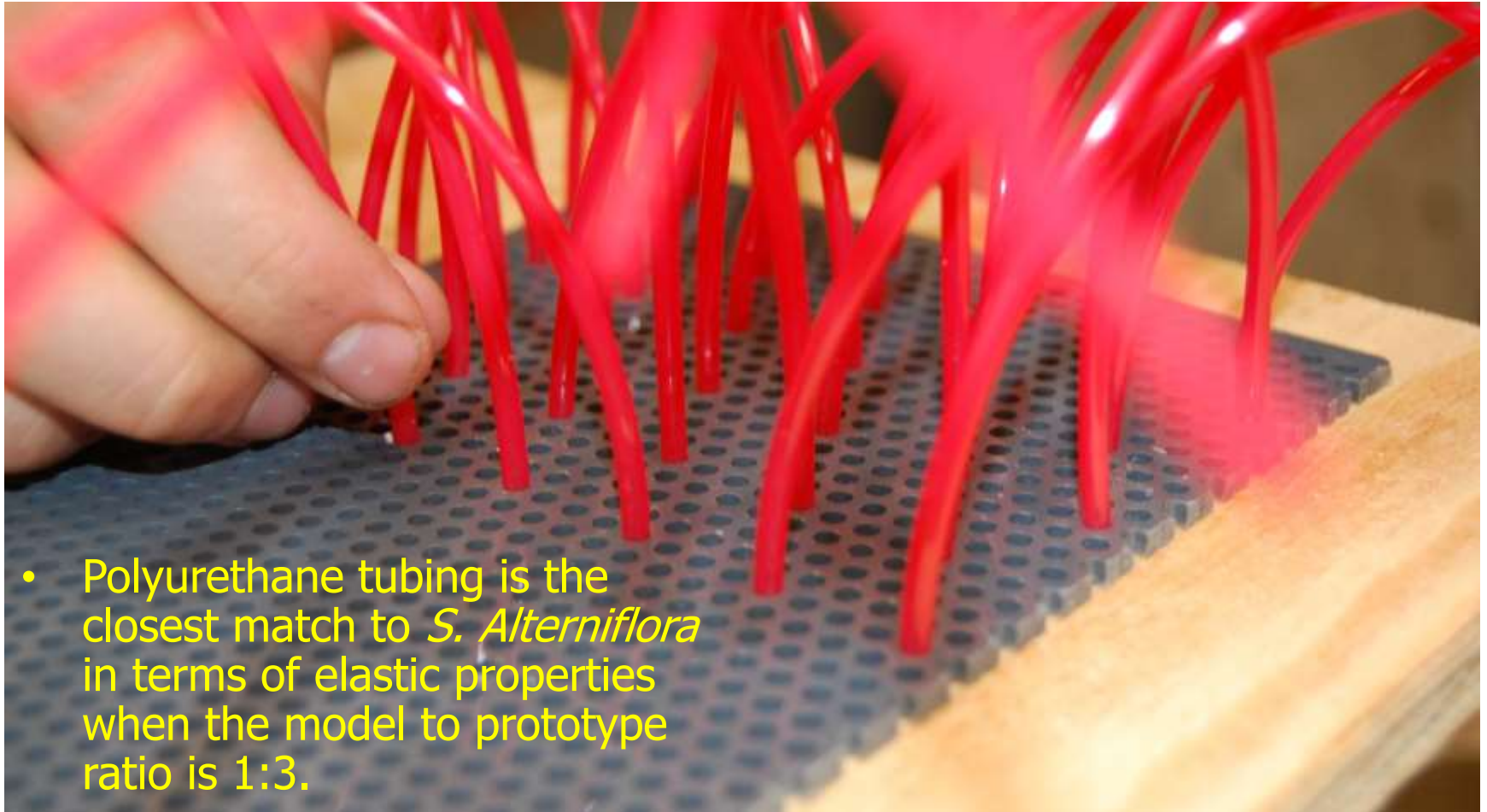
Wave Runup Experiment using Rigid Model Vegetation



Wave Runup Experiment using Flexible Model Vegetation



Flexible Model Vegetation



- Polyurethane tubing is the closest match to *S. Alterniflora* in terms of elastic properties when the model to prototype ratio is 1:3.

	EPDM rubber	Polyurethane	Model	Prototype
E (GPa)	3.86E-03	3.59E-02	9.46E-02	2.83E-01 (LSU team)
EI (Nt*m²)	1.60E-05	1.41E-04	1.17E-04	2.84E-02 (Feagin, 2010)

Computational Modeling of Wave Attenuation by Vegetation

Models Used for Wave Attenuation

- 1-D/2-D shallow water flow models with HLL approximate Riemann solver ([Wu and Marsooli, 2012](#))
- 1-D Boussinesq wave model
- 2-D vertical Navier-Stokes model with VOF
- 3-D Navier-Stokes models with VOF ([Marsooli and Wu, 2014](#))
- 2-D spectral wave transformation model
- 3-D shallow water model coupled with spectral wave transformation model ([Wu, 2014](#))

Depth-Averaged 2-D Model for Long Waves

(Wu and Marsooli, 2012)

Governing equations:

$$\frac{\partial h}{\partial t} + \frac{\partial(Uh)}{\partial x} + \frac{\partial(Vh)}{\partial y} = 0$$

$$\frac{\partial}{\partial t}(Uh) + \frac{\partial}{\partial x}(U^2h) + \frac{\partial}{\partial y}(UVh) = -\frac{1}{\rho}F_x - gh\frac{\partial\eta}{\partial x} + \frac{\partial}{\partial x}\left(v_t h \frac{\partial U}{\partial x}\right) + \frac{\partial}{\partial y}\left(v_t h \frac{\partial U}{\partial y}\right) - g\frac{n^2 m_b U \bar{U}}{h^{1/3}}$$

$$\frac{\partial}{\partial t}(Vh) + \frac{\partial}{\partial x}(UVh) + \frac{\partial}{\partial y}(V^2h) = -\frac{1}{\rho}F_y - gh\frac{\partial\eta}{\partial y} + \frac{\partial}{\partial x}\left(v_t h \frac{\partial V}{\partial x}\right) + \frac{\partial}{\partial y}\left(v_t h \frac{\partial V}{\partial y}\right) - g\frac{n^2 m_b V \bar{U}}{h^{1/3}}$$

Drag and inertia forces::

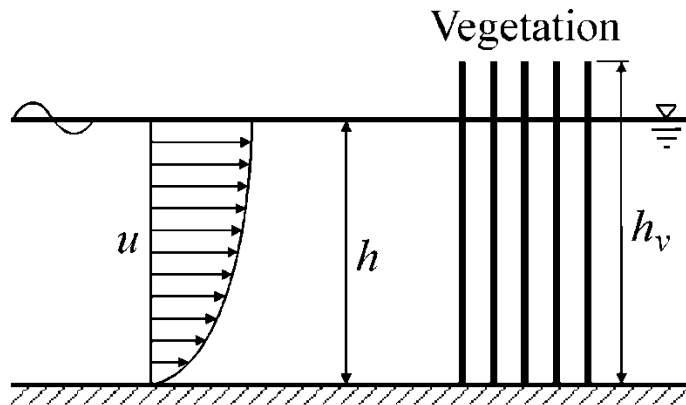
$$F_i = \frac{1}{2}\rho C_D N_v A_v U_{vi} \sqrt{U_{vj} U_{vj}} + \rho C_M N_v V_v \frac{\partial U_{vi}}{\partial t}$$

Drag Force of Submerged Vegetation

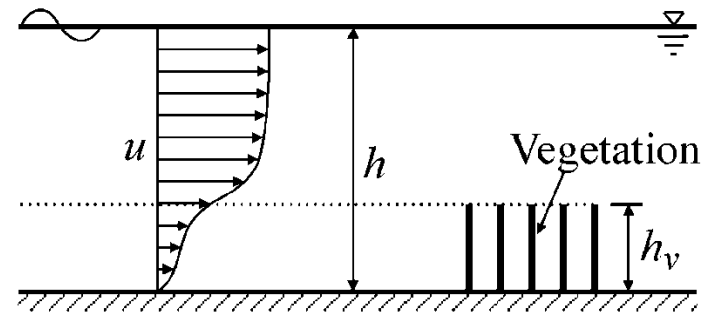
$$\vec{F}_D = \frac{1}{2} C_D \rho N_v A_v |\bar{U}_v| \vec{U}_v$$

For submerged vegetation, Stone and Shen's (2002) method:

$$U_v = \eta_v \left(\frac{h_v}{h} \right)^{0.5} U$$



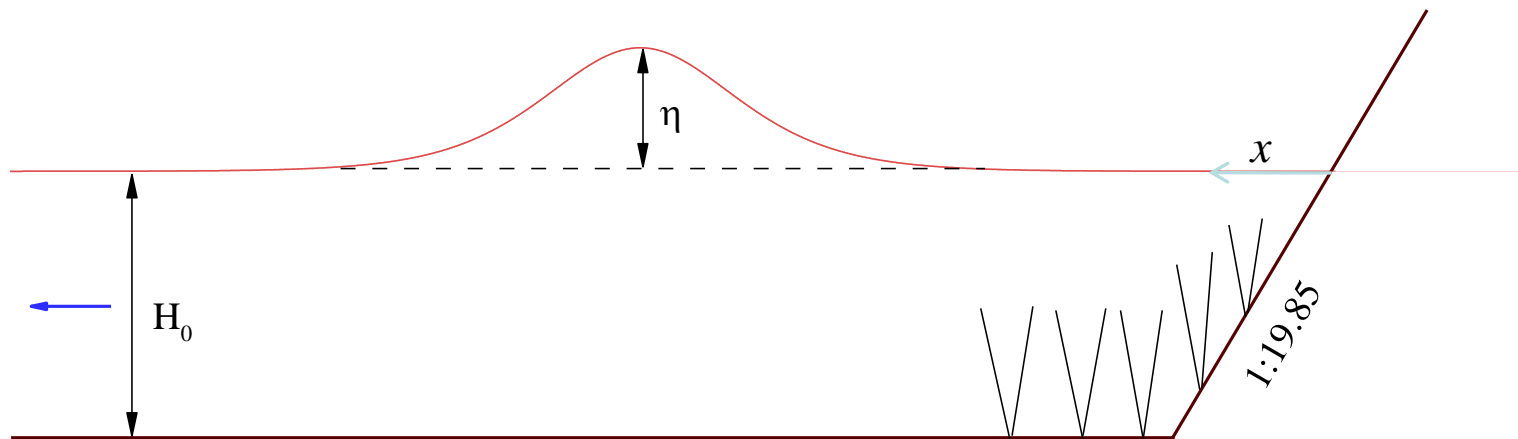
(a) Emergent



(b) Submerged

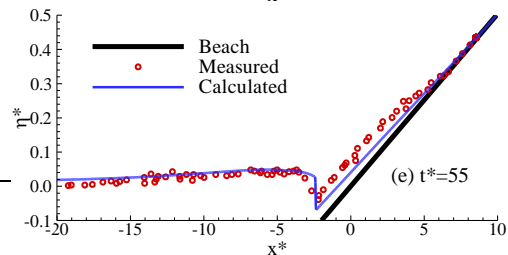
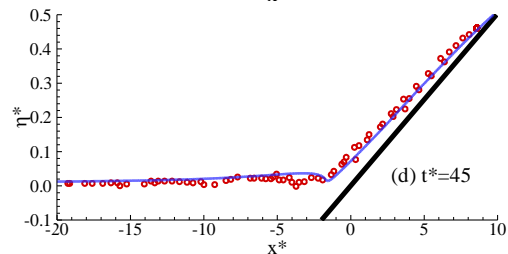
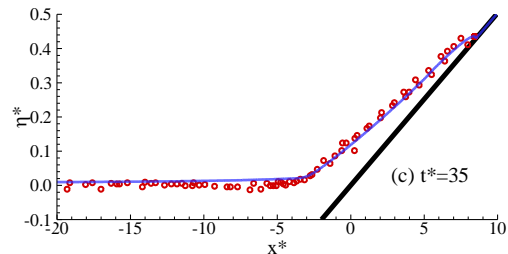
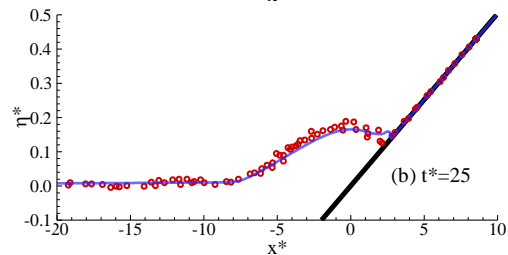
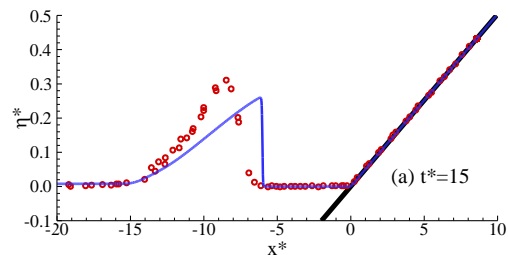
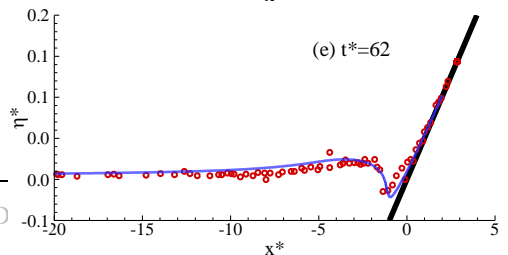
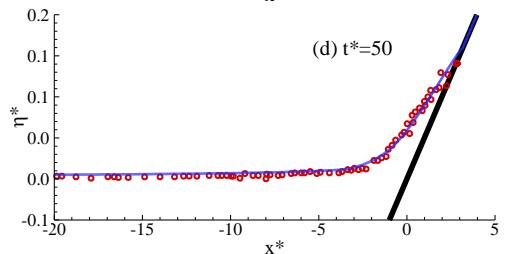
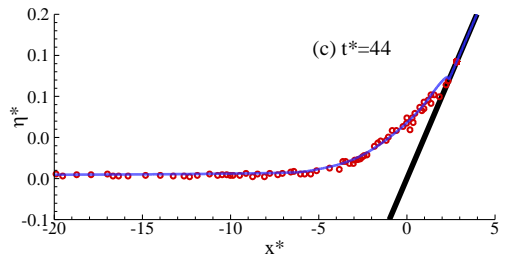
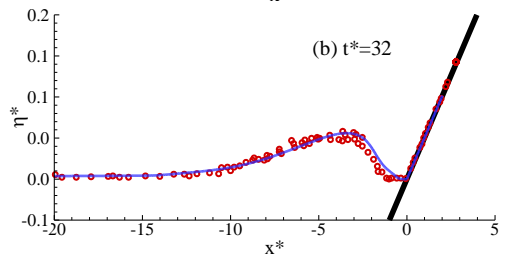
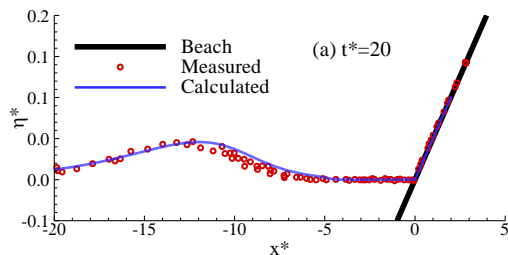
Solitary Wave Run-up (SWE Model)

Experimental study: Synolakis (1986)



- (a) Non-breaking wave for $H/H_0 = 0.0185$
- (b) Non-breaking wave for $H/H_0 = 0.04$
- (c) Breaking wave for $H/H_0 = 0.3$

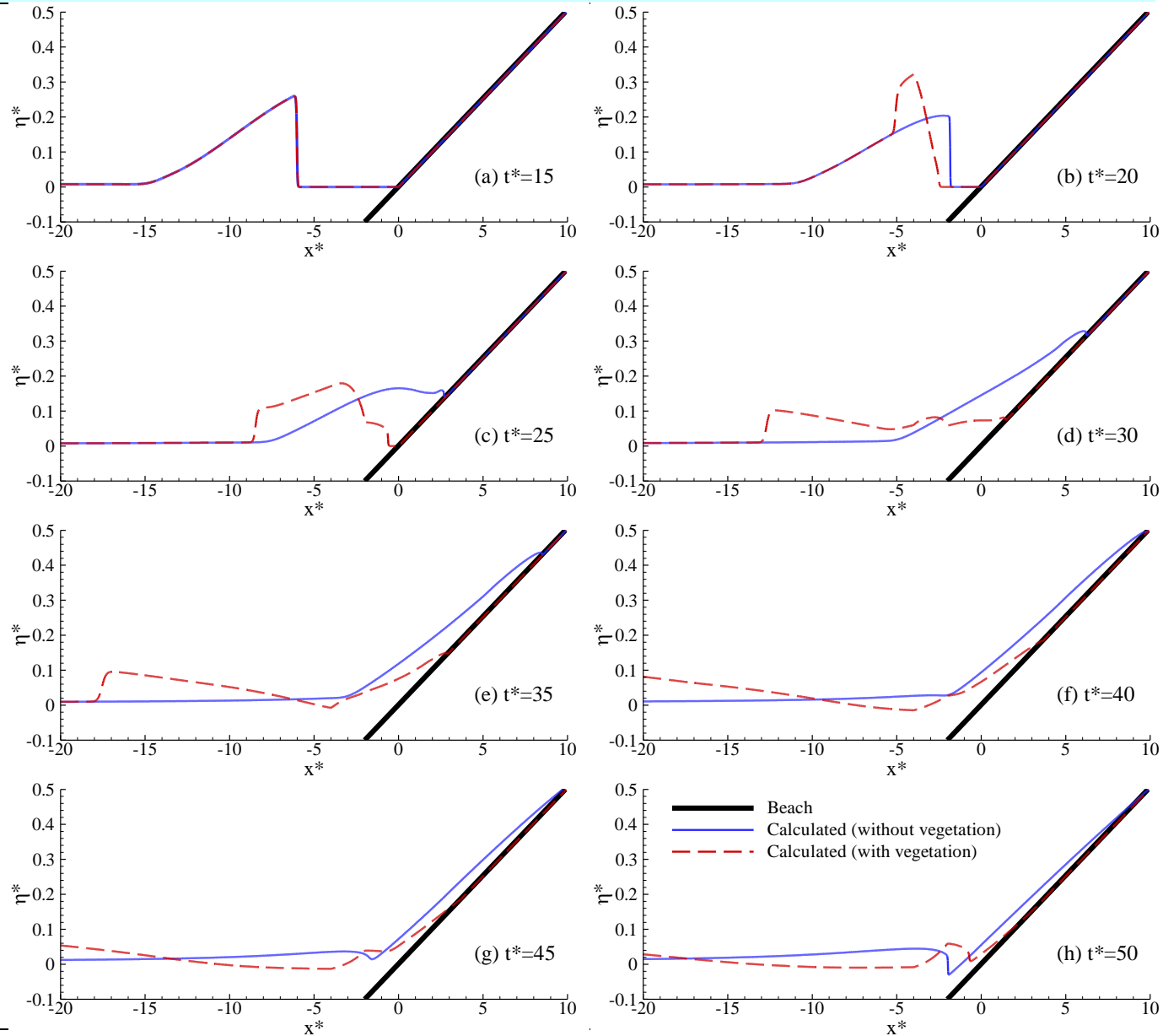
Non-Breaking and Breaking Wave Run-up over a Breach



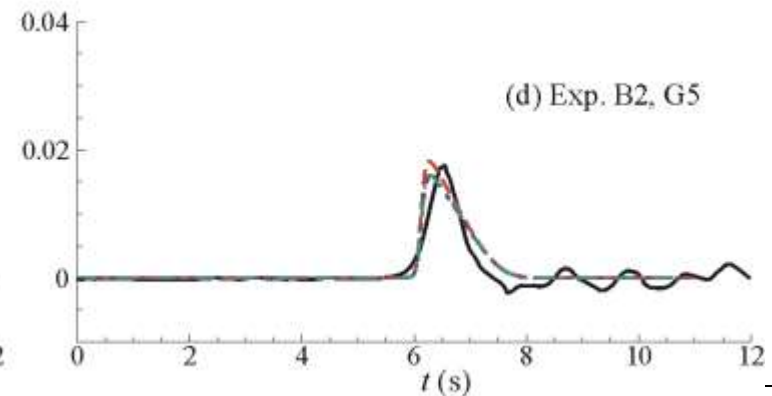
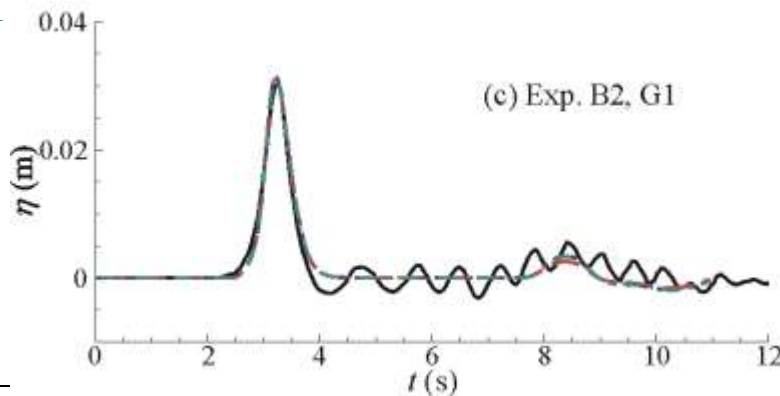
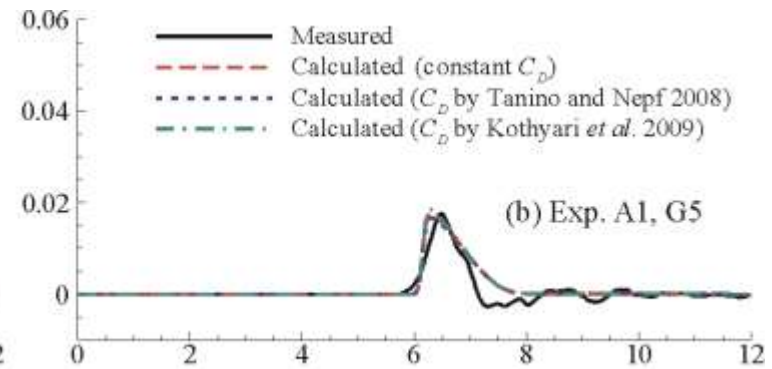
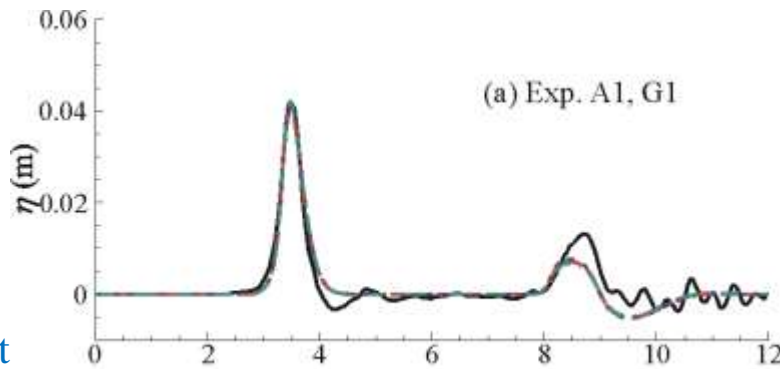
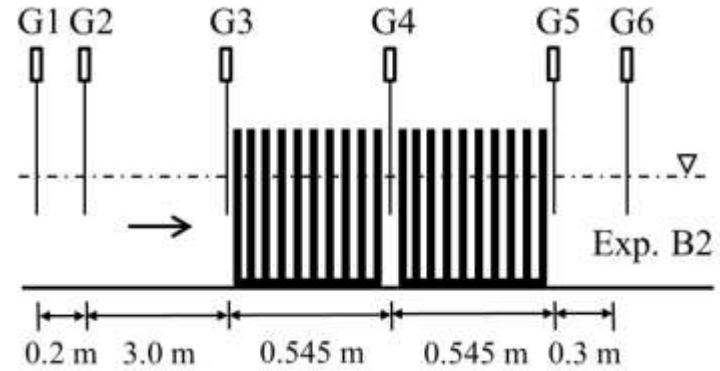
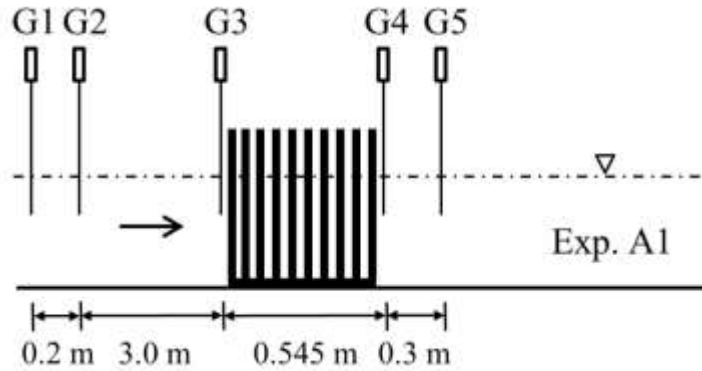
Run-up of $H/H_0 = 0.04$ solitary wave on 1:19.85 sloping beach

Run-up of $H/H_0 = 0.3$ solitary wave on 1:19.85 sloping beach

Breaking Wave Run-up on Vegetated Beach



Solitary Wave through Vegetated Channel



Wave heights at gages G1 and G5

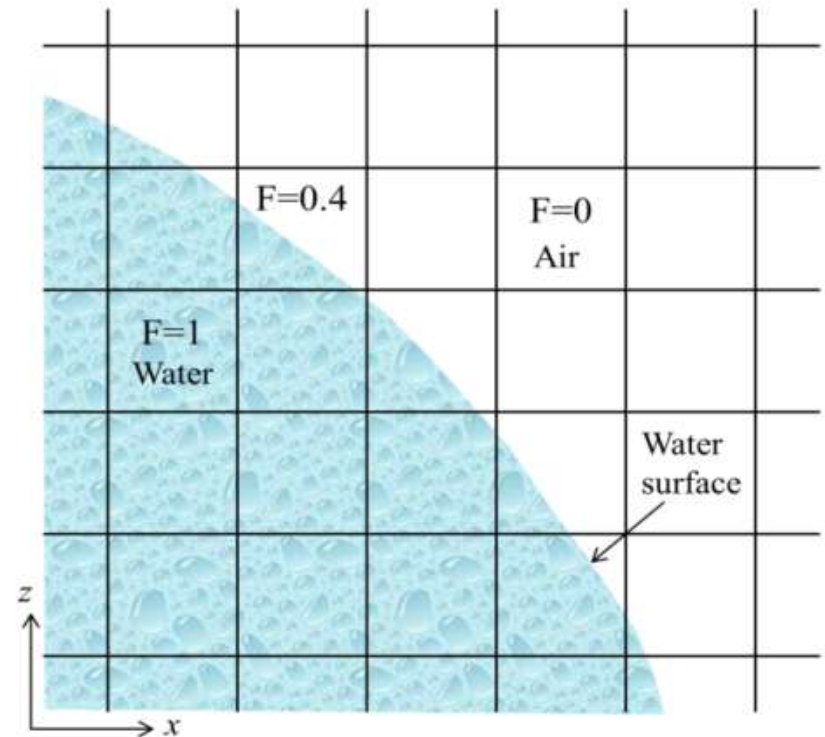
3-D RANS Model with VOF (Marsooli and Wu, 2014)

$$\nabla \cdot \mathbf{u} = 0$$

$$\frac{\partial \mathbf{u}}{\partial t} + \nabla \cdot (\mathbf{u}\mathbf{u}) = -\frac{1}{\rho} \nabla p + \frac{1}{\rho} \mathbf{f} + \frac{1}{\rho} \nabla \cdot (\mu \nabla \mathbf{u})$$

$$\frac{\partial F}{\partial t} + \nabla \cdot (F\mathbf{u}) = 0$$

- Empty cell: $F=0$
- Fluid cell: $F=1$
- Surface cell: $0 < F < 1$



Drag and Inertia Forces of Vegetation

$$f_i = \frac{1}{2} \rho C_{D(i)} N_v b_v u_i \sqrt{u_j u_j} + \rho C_M N_v s_v \frac{\partial u_i}{\partial t}$$

where C_D = drag coefficient

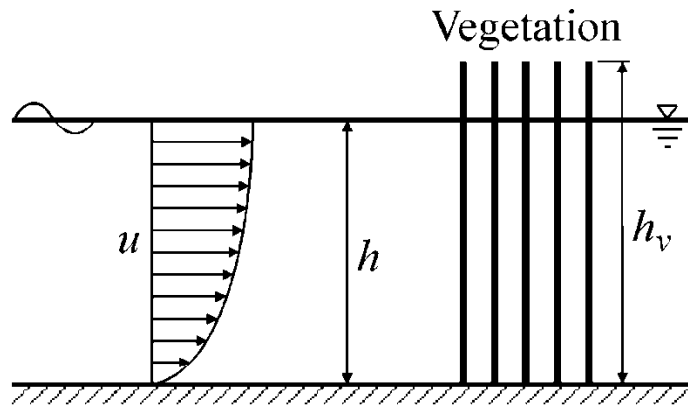
C_M = inertia coefficient

N_v = density of vegetation (units/m²)

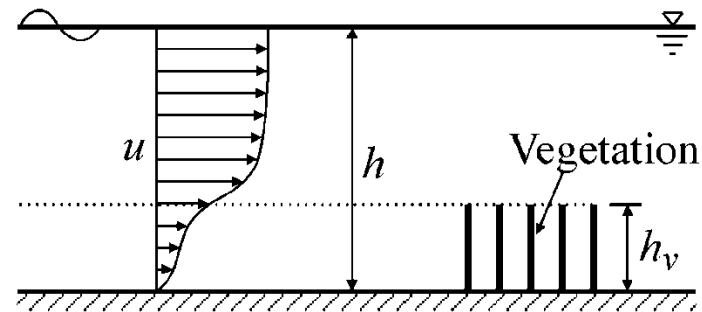
b_v = front width of vegetation stem

s_v = horizontal coverage area of vegetation

ρ = fluid density

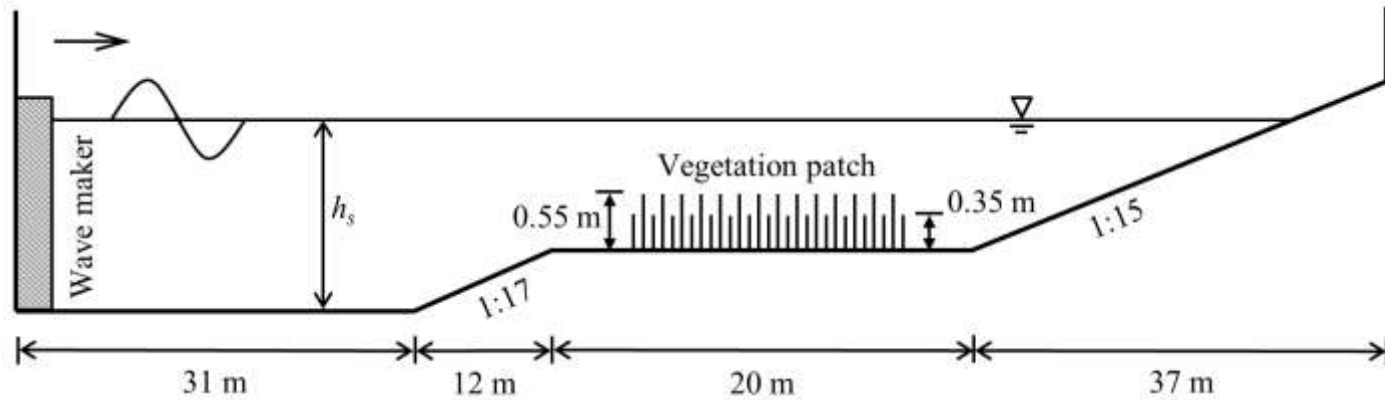


(a) Emergent



(b) Submerged

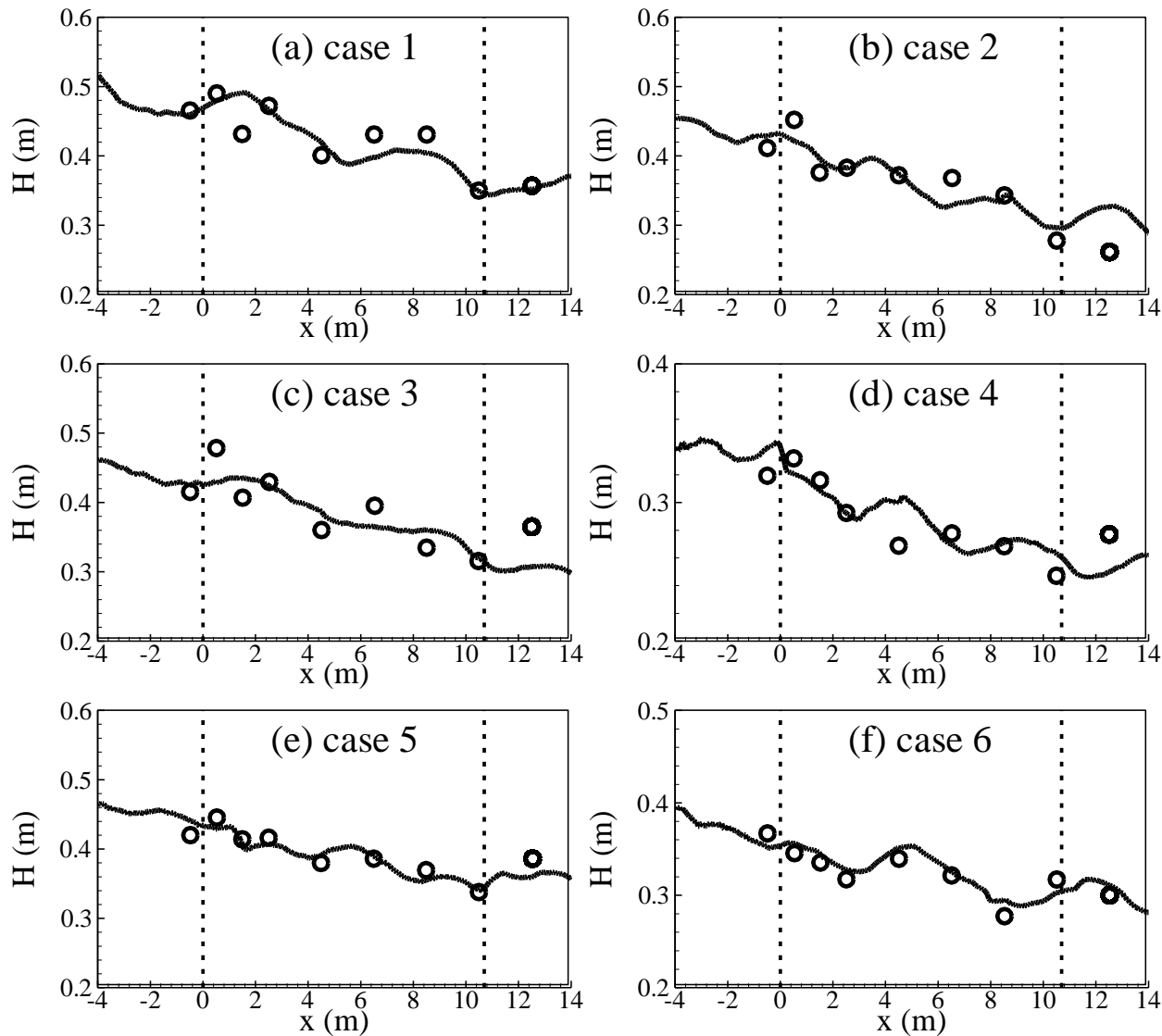
Test of 3-D RANS Model



Experimental runs of Stratigaki et al. (2011) tested by the present model

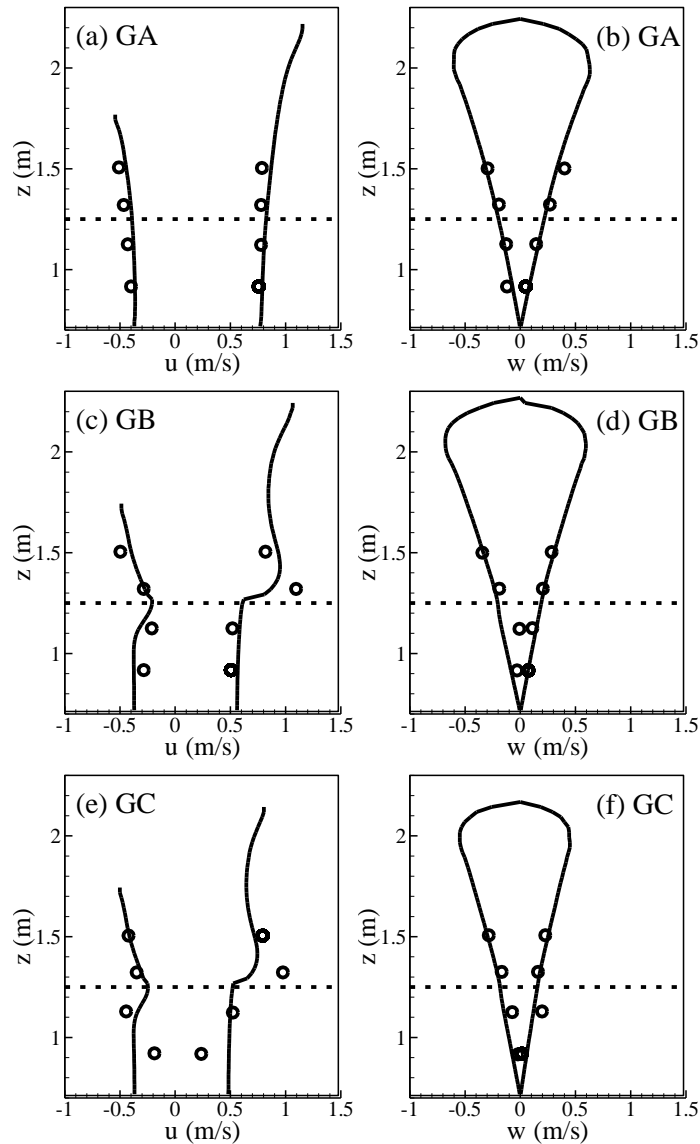
Case	Still water depth h_s (m)	Incident wave height H_i (m)	Wave period T (s)	Vegetation density N_v (stems/m ²)	Calibrated C_D
1	1.8	0.44	4.0	360	0.8
2	1.8	0.44	3.0	360	0.9
3	2.0	0.43	3.5	360	1.6
4	2.0	0.33	3.0	360	1.0
5	2.2	0.44	3.0	360	1.0
6	2.4	0.36	3.0	180	1.9

Test of 3-D RANS Model



Calculated (solid line) and Stratigaki et al. (2011) experimental (circles) wave height profiles inside the vegetation patch. x denotes the longitudinal distance from the upstream edge of the vegetation patch; vertical dashed lines denote the boundaries of the vegetation patch.

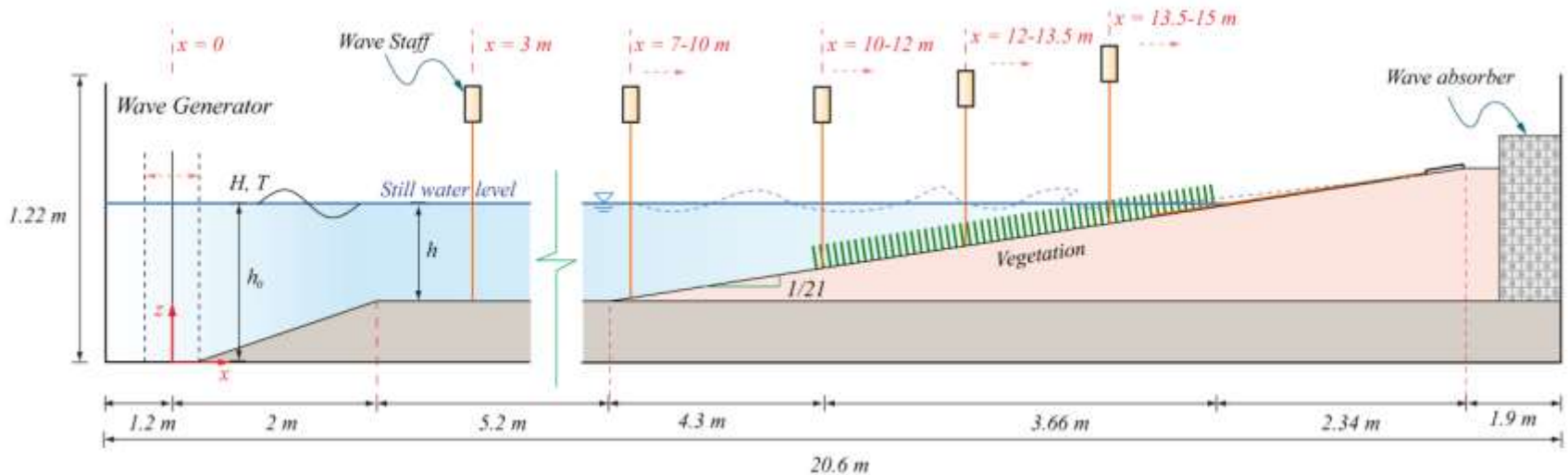
Test of 3-D RANS Model



Calculated (solid line) and Stratigaki et al. (2011) experimental (circles) vertical profiles of maximum and minimum stream-wise, u , and vertical, w , velocities for case 1; Horizontal dashed line denotes the vegetation height.

Points GA, GB, and GC are located 0.7 m upstream of the upper meadow edge, 2 m downstream of the upper meadow edge, and 2.7 m upstream of the lower meadow edge, respectively.

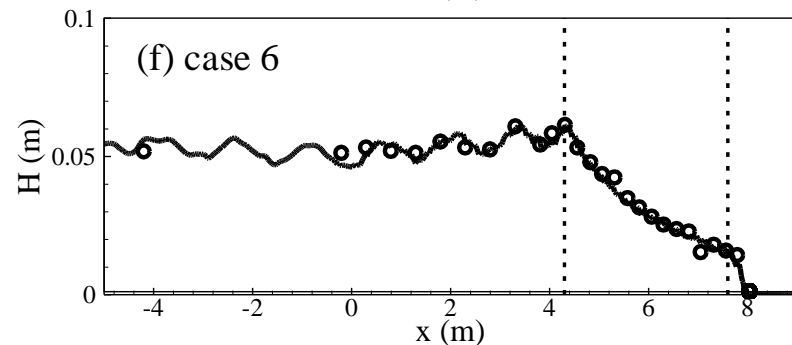
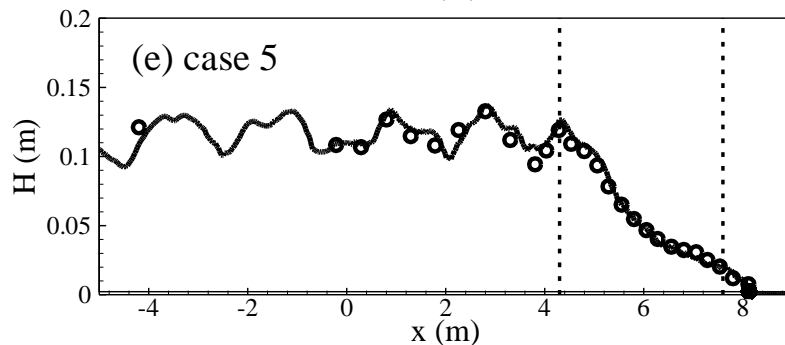
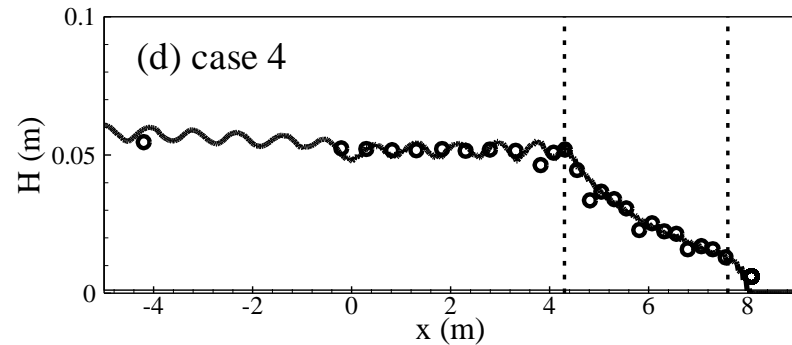
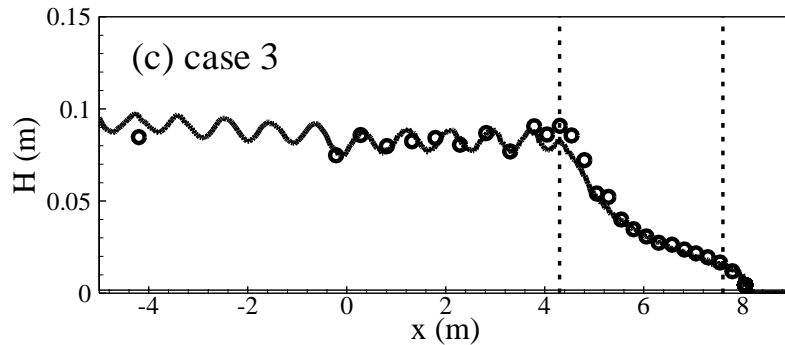
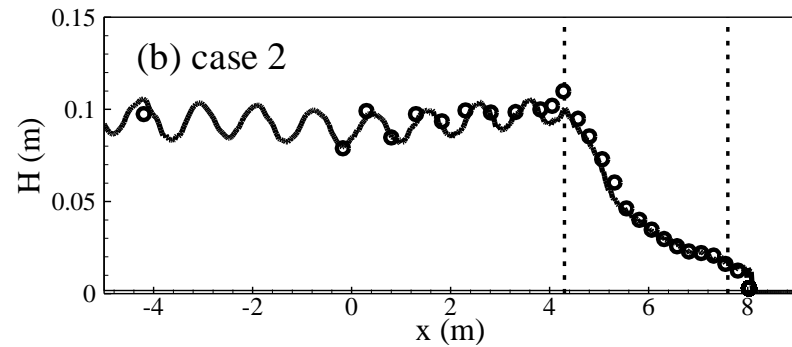
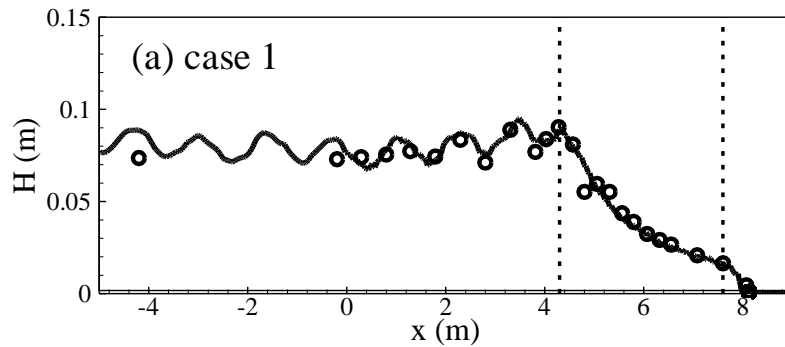
Test of 3-D RANS Model



Case	Vegetation type	Still water depth h_s (m)	Incident wave height H_i (m)	Wave period T (s)	Calibrate d C_D
1	rigid	0.4	0.0757	1.6	1.7
2	rigid	0.4	0.0931	1.4	1.7
3	rigid	0.4	0.0873	1.2	1.7
4	rigid	0.4	0.0551	1.2	1.7
5	rigid	0.4	0.1200	2.4	1.7
6	rigid	0.4	0.0533	1.8	1.7
7	flexible	0.4	0.0757	1.6	1.0
8	flexible	0.4	0.0931	1.4	1.0
9	flexible	0.4	0.0873	1.2	1.3
10	flexible	0.4	0.0551	1.2	1.4
11	flexible	0.4	0.1200	2.4	1.1
12	flexible	0.4	0.0533	1.8	1.2

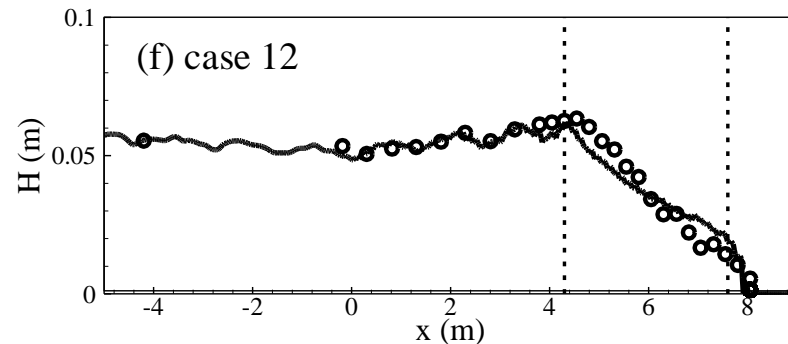
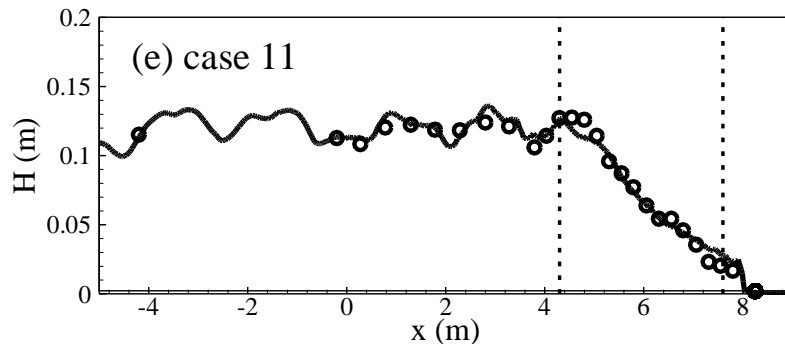
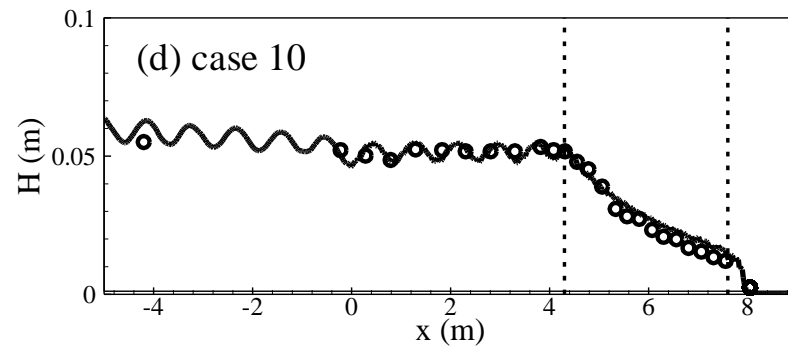
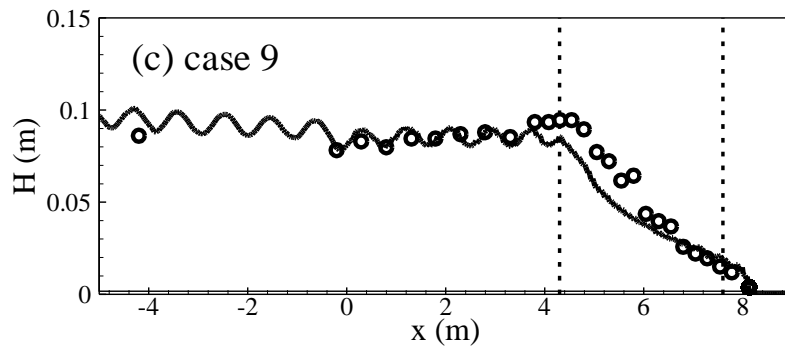
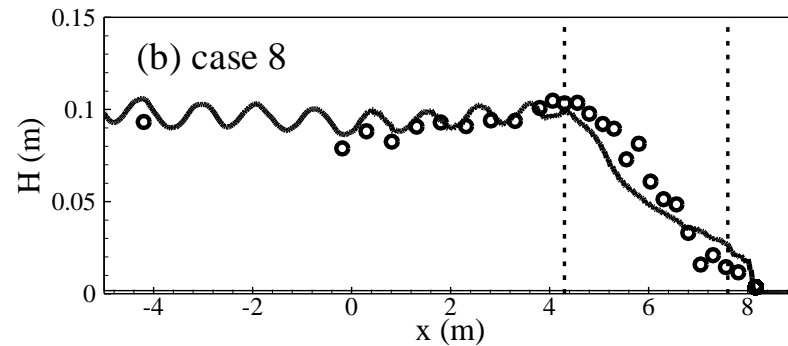
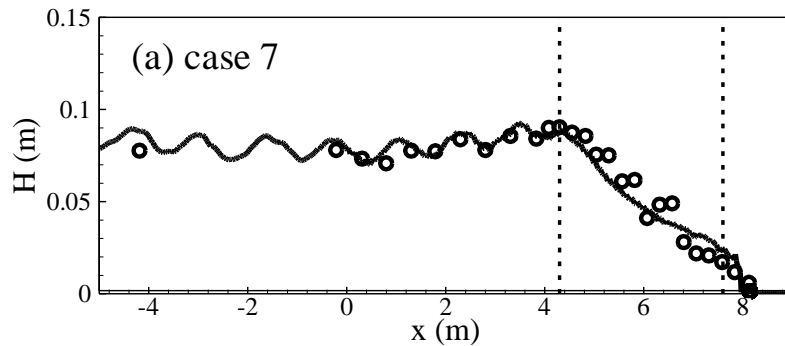
Experimental runs of NSL experiments over sloping bed tested by the present model

Test of 3-D RANS Model



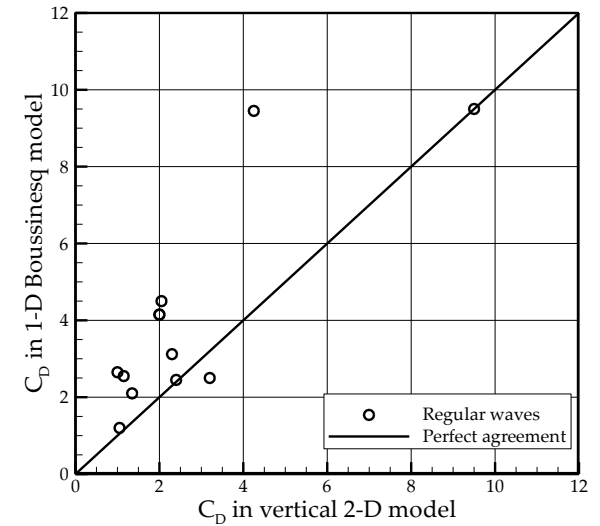
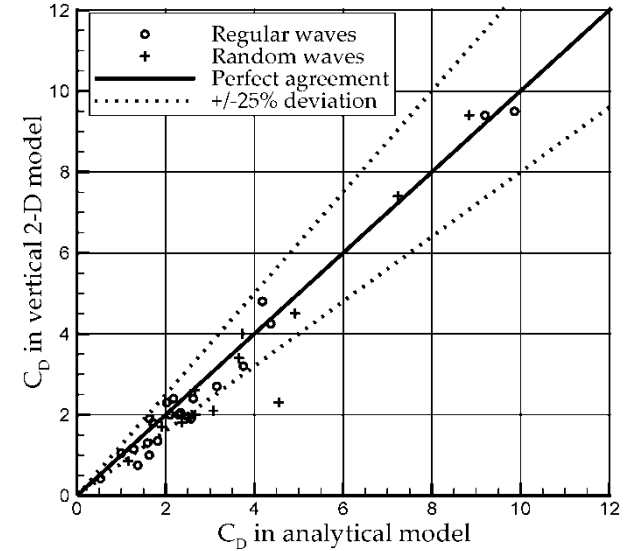
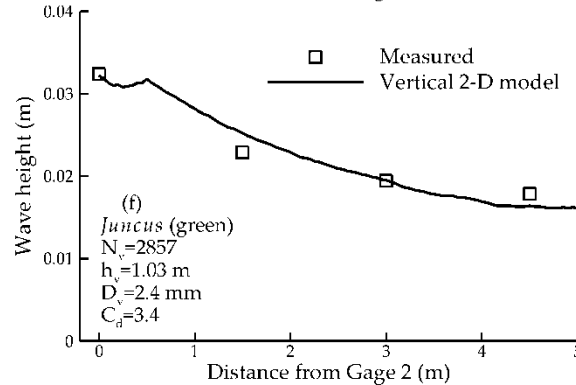
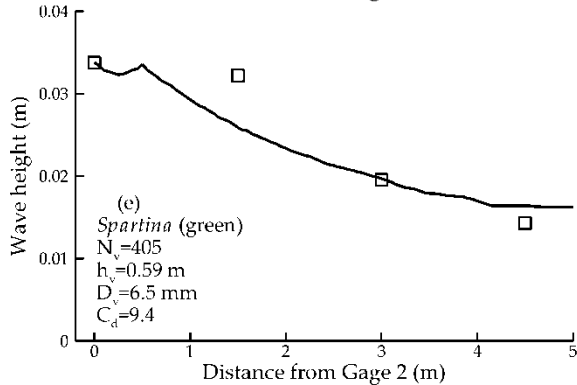
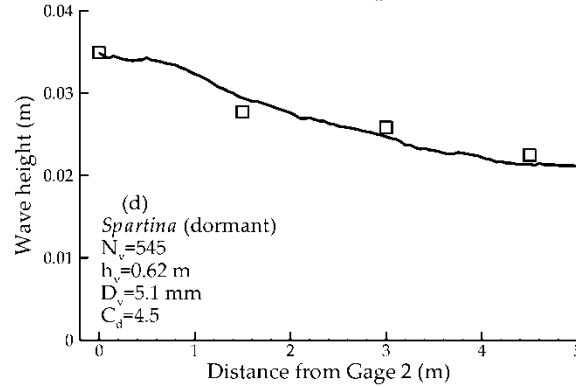
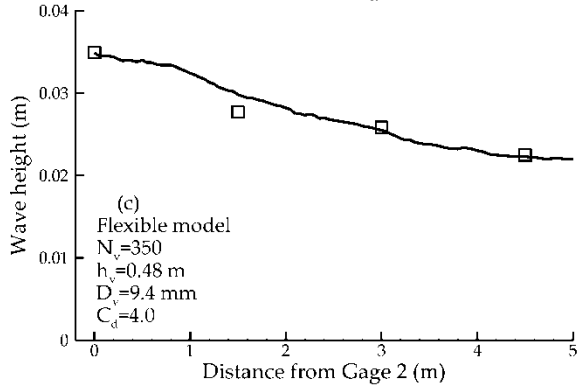
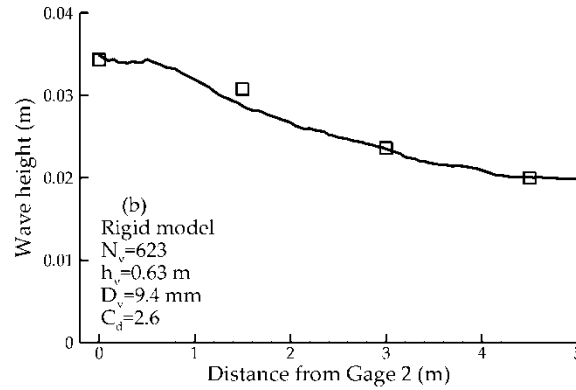
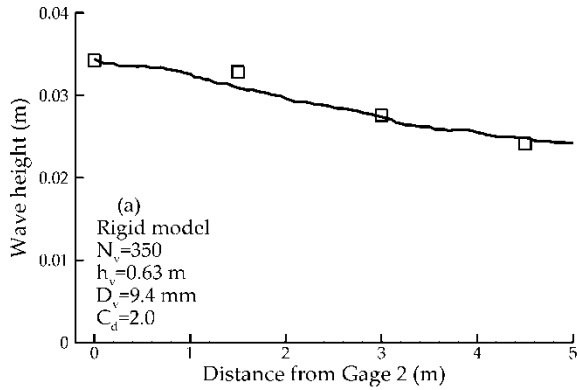
Calculated (solid line) and NSL experimental (circles) wave height profiles inside the vegetation patch for rigid vegetation and sloping bed. x denotes the longitudinal distance from the toe of sloping bed; vertical dashed lines denote the boundaries of the vegetation patch.

Test of 3-D RANS Model



Calculated (solid line) and NSL experimental (circles) wave height profiles inside the vegetation patch for flexible vegetation and sloping bed. x denotes the longitudinal distance from the toe of sloping bed; vertical dashed lines denote the boundaries of the vegetation patch.

Random Waves through Vegetated Flume



Calculated by RANS model (Wu et al. 2013)

3-D Phase-Averaged Shallow Water Flow Model

(Wu, 2014)

Governing equations:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

$$\begin{aligned} \frac{\partial u}{\partial t} + \frac{\partial(uu)}{\partial x} + \frac{\partial(vu)}{\partial y} + \frac{\partial(wu)}{\partial z} = & -\frac{1}{\rho} \frac{\partial p_a}{\partial x} - \frac{1}{\rho} \left(\rho_0 g \frac{\partial \eta}{\partial x} + g \int_z^\eta \frac{\partial \rho}{\partial x} dz \right) \\ & + \frac{\partial}{\partial x} \left(\nu_{tH} \frac{\partial u}{\partial x} \right) + \frac{\partial}{\partial y} \left(\nu_{tH} \frac{\partial u}{\partial y} \right) + \frac{\partial}{\partial z} \left(\nu_{tV} \frac{\partial u}{\partial z} \right) - \frac{1}{\rho} \frac{\partial S_{xx}}{\partial x} - \frac{1}{\rho} \frac{\partial S_{xy}}{\partial y} - \frac{1}{\rho} f_x + f_c v \end{aligned}$$

$$\begin{aligned} \frac{\partial v}{\partial t} + \frac{\partial(uv)}{\partial x} + \frac{\partial(vv)}{\partial y} + \frac{\partial(wv)}{\partial z} = & -\frac{1}{\rho} \frac{\partial p_a}{\partial y} - \frac{1}{\rho} \left(\rho_0 g \frac{\partial \eta}{\partial y} + g \int_z^\eta \frac{\partial \rho}{\partial y} dz \right) \\ & + \frac{\partial}{\partial x} \left(\nu_{tH} \frac{\partial v}{\partial x} \right) + \frac{\partial}{\partial y} \left(\nu_{tH} \frac{\partial v}{\partial y} \right) + \frac{\partial}{\partial z} \left(\nu_{tV} \frac{\partial v}{\partial z} \right) - \frac{1}{\rho} \frac{\partial S_{yx}}{\partial x} - \frac{1}{\rho} \frac{\partial S_{yy}}{\partial y} - \frac{1}{\rho} f_y - f_c u \end{aligned}$$

Eddy viscosity:

$$\nu_t = \sqrt{\left(l_{mV}^2 |\bar{S}_V|\right)^2 + \left(l_{mH}^2 |\bar{S}_H|\right)^2}$$

where $|\bar{S}_V|$ and $|\bar{S}_H|$ are shear strains in the vertical and horizontal directions; l_{mV} is the vertical mixing length: $=\kappa z(1-z/h)^{1/2}$ when $z < 2h/3$ and $=2\kappa h/3^{3/2}$ when $z \geq 2h/3$; and l_{mH} is the horizontal mixing length $=\kappa \min(l, c_m h)$. Here, z is the vertical coordinate above the bed, l is the horizontal distance to the nearest solid wall, h is the flow depth, κ is the von Karman constant, and c_m is a coefficient which is set as about 0.3 in this study.

Bed shear stress

$$\tau_{bx} = \rho c_f u_b \sqrt{u_b^2 + v_b^2 + 0.5U_{wm}^2}, \quad \tau_{by} = \rho c_f v_b \sqrt{u_b^2 + v_b^2 + 0.5U_{wm}^2}$$

where u_b and v_b are the x - and y -velocities near the bed; c_f is the bed friction coefficient; and U_{wm} is the maximum orbital bottom velocity of wave.

Spectral wave-action balance equation (Mase et al. 2005):

$$\frac{\partial N}{\partial t} + \frac{\partial(c_x N)}{\partial x} + \frac{\partial(c_y N)}{\partial y} + \frac{\partial(c_\theta N)}{\partial \theta} = \frac{\kappa_w}{2\sigma} \left[\frac{\partial}{\partial y} \left(CC_g \cos^2 \theta \frac{\partial N}{\partial y} \right) - \frac{1}{2} CC_g \cos^2 \theta \frac{\partial^2 N}{\partial y^2} \right] - \varepsilon_b N - Q_v + Q$$

where $N = E(x,y,\sigma,\theta,t)/\sigma$; E is the spectral wave density representing the wave energy per unit water surface area per frequency interval; σ is the wave angular frequency (or intrinsic frequency); θ is the wave angle relative to the positive x -direction; C and C_g are wave celerity and group velocity, respectively; c_x , c_y , and c_θ are the characteristic velocities with respect to x , y and θ , respectively; κ_w is an empirical coefficient; ε_b is a parameter for wave breaking energy dissipation; Q_v represents the wave energy loss due to vegetation resistance; and Q includes source/sink terms of wave energy due to wind forcing, bottom friction loss, nonlinear wave-wave interaction, etc.

$$c_x = C_g \cos \theta + U \quad c_y = C_g \sin \theta + V$$

$$c_\theta = \frac{\sigma}{\sinh 2kh} \left(\sin \theta \frac{\partial h}{\partial x} - \cos \theta \frac{\partial h}{\partial y} \right) + \cos \theta \sin \theta \frac{\partial U}{\partial x} - \cos^2 \theta \frac{\partial U}{\partial y} + \sin^2 \theta \frac{\partial V}{\partial x} - \sin \theta \cos \theta \frac{\partial V}{\partial y}$$

Wave Energy Dissipation by Vegetation (Mendez and Losada, 2004)

Assumptions:

- (1) Linear waves
- (2) Impermeable bottom
- (3) Invariant Rayleigh wave height distribution
- (4) Thornton and Guza's wave breaking criteria
- (5) Without current

$$Q_v = \frac{1}{2\sqrt{\pi}} \rho C_D b_v N_v \left(\frac{kg}{2\sigma} \right)^3 \frac{\sinh^3(k\alpha h) + 3\sinh(k\alpha h)}{3k \cosh^3(kh)} H_{rms}^3$$

H_{rms} = root-mean-square wave height (m)

Total Energy Loss by Vegetation in Case of Currents and Waves Coexisted

$$Q_{tv} = \frac{1}{T} \int_0^T \int_0^{h_v} F_i u_{cwi} dz dt \approx \frac{1}{T} \int_0^T \int_0^{h_v} F_x u_{cw} dz dt = \frac{1}{T} \int_0^T \int_0^{h_v} \frac{1}{2} \rho C_D N_v b_v u_{cw}^3 dz dt$$

Consider $u_{cw} = u_c + u_w$

$$Q_{tv} = \frac{1}{T} \int_0^T \int_0^{h_v} \frac{1}{2} \rho C_D N_v b_v u_c^3 dz dt + \frac{1}{T} \int_0^T \int_0^{h_v} \frac{3}{2} \rho C_D N_v b_v u_c u_w^2 dz dt + \frac{1}{T} \int_0^T \int_0^{h_v} \frac{1}{2} \rho C_D N_v b_v u_w^3 dz dt$$

Due to current

Related to both current and waves

Due to waves

Considered thru drag force in the momentum equations



Considered thru wave energy dissipation in wave-action balance equation

Wave Dissipation by Vegetation in Case of Currents and Waves Coexisted

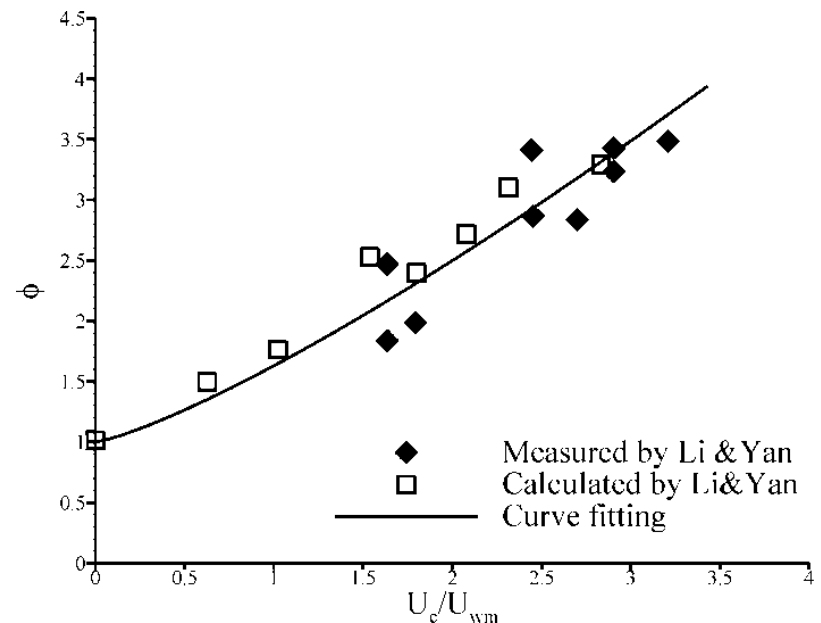
The method of Mendez and Losada is modified as

$$Q_v = \frac{1}{\sigma 2\sqrt{\pi}} \rho C_D \phi b_v N_v \left(\frac{kg}{2\sigma} \right)^3 \frac{\sinh^3(kh_v) + 3\sinh(kh_v)}{3k \cosh^3(kh)} H_{rms}^3$$

by introducing a correction factor:

$$\phi = 1 + a \left(\frac{U_c}{U_{wm}} \right)^m$$

where U_c is the current velocity and U_{wm} is the maximum orbital bottom velocity of wave. $m=1.25$ and $a=0.63$, which are approximated using Li and Yan's (2007) data.



Wave Radiation Stress

Formula of Mellor (2008)

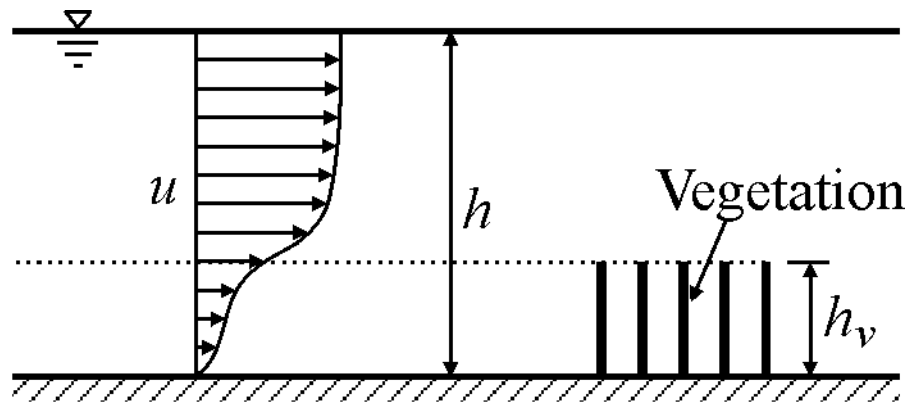
$$S_{ij} = \int_0^\infty \int_{-\pi}^\pi \left\{ k(f)E(f, \theta) \left[\frac{k_i(f)k_j(f)}{k(f)^2} \frac{\cosh^2 k(h+z')}{\sinh kD \cosh kD} - \delta_{ij} \frac{\sinh^2 k(h+z')}{\sinh kD \cosh kD} \right] + \delta_{ij} E_D(f, \theta) \right\} d\theta df$$

where E is the wave energy, k is the wave number, θ is the angle of wave propagation to the onshore direction, f is the wave frequency, h is the still water depth, D is the total water depth, z' is the vertical coordinate referred to the still water level, and E_D is a modified Dirac delta function which is 0 if $z \neq \eta$ and has the following quantity:

$$\int_{-h}^{\eta^+} E_D dz = E / 2$$

Flow in Channel with Submerged Vegetation

Experiment by Lopez and Garcia (1997)

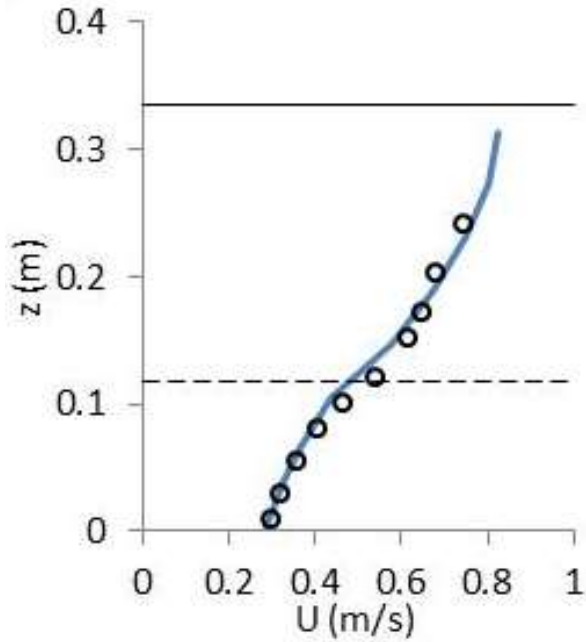


Rigid: Wooden cylinders

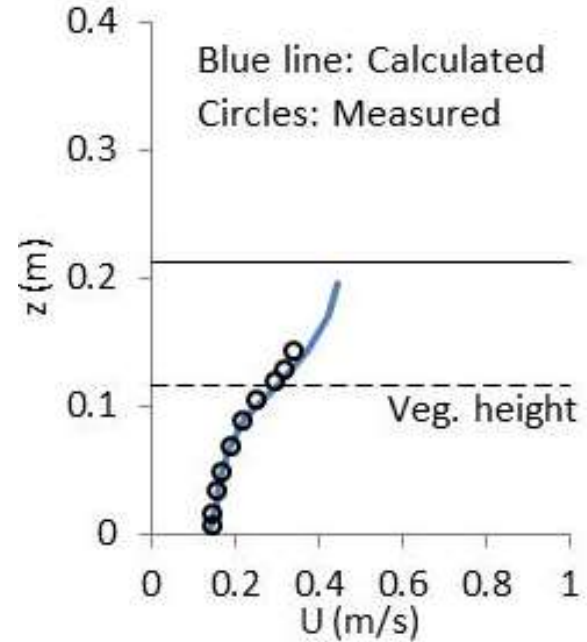
Flexible: Plastic drinking straws

Exp. No.	Discharge (m ³ /s)	Flow depth (m)	Bed slope	Vegetation type	$N_v D_v$ (1/m)	Vegetation height (m)	Drag coefficient
1	0.179	0.335	0.0036	Rigid	1.09	0.1175	1.1
9	0.058	0.214	0.0036	Rigid	2.46	0.1175	1.1
13	0.179	0.368	0.0036	Flexible	1.09	0.152	1.2
17	0.078	0.279	0.0036	Flexible	2.46	0.16	1.3

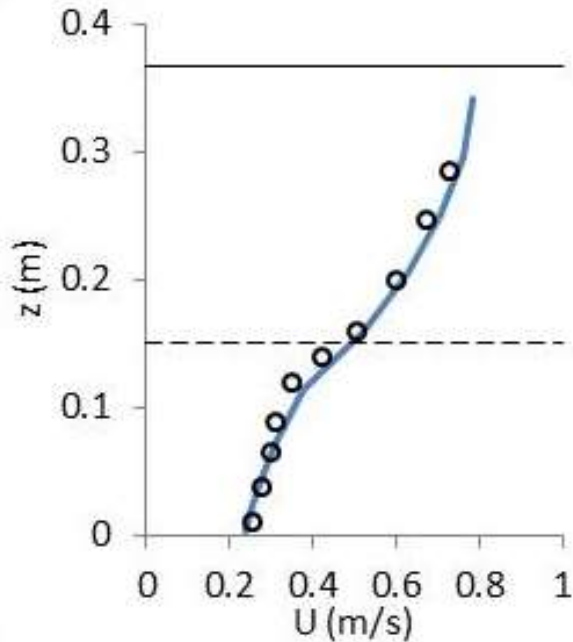
No. 1



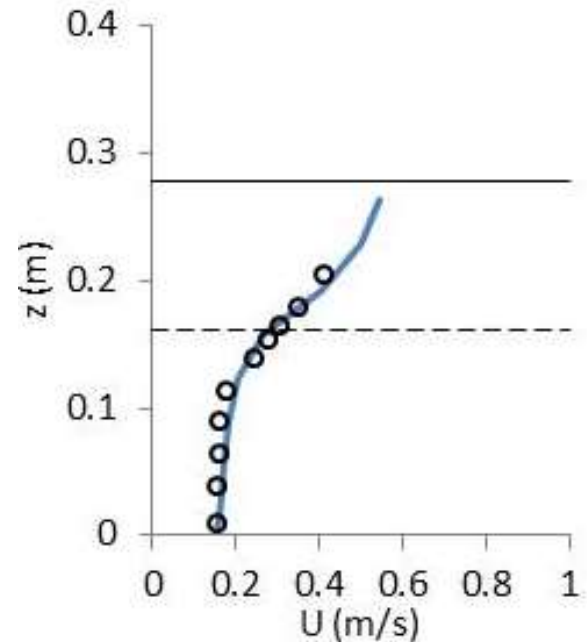
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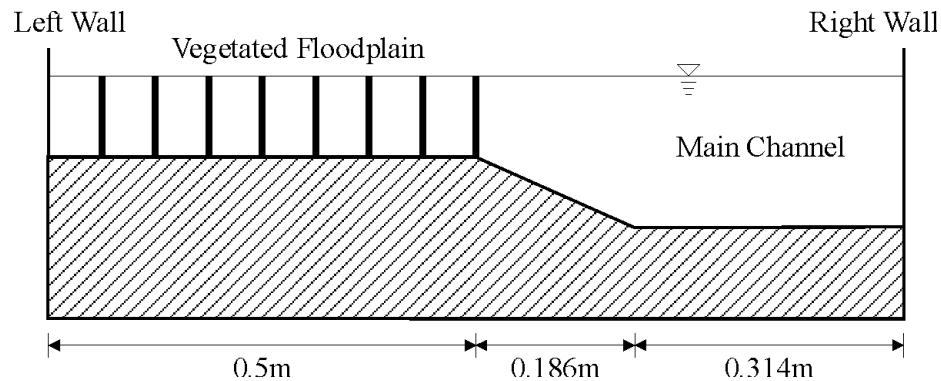
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No. 17



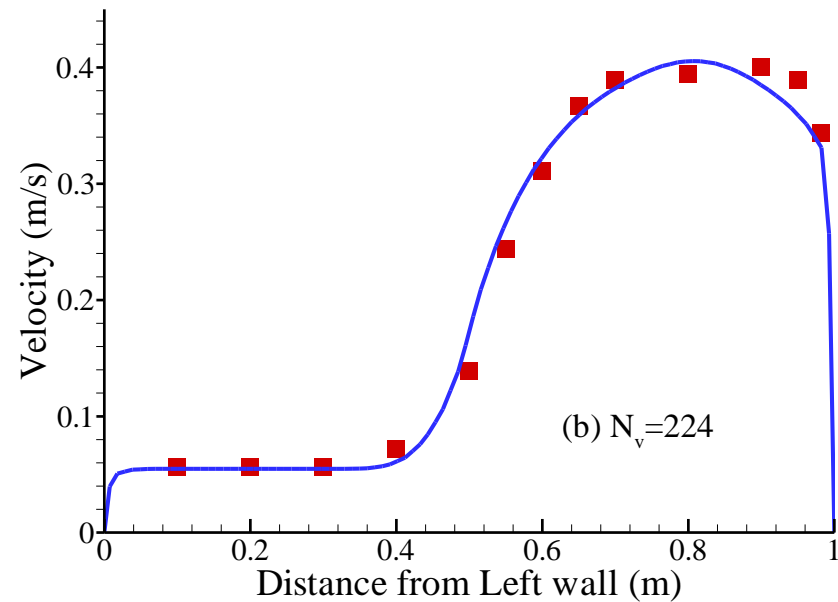
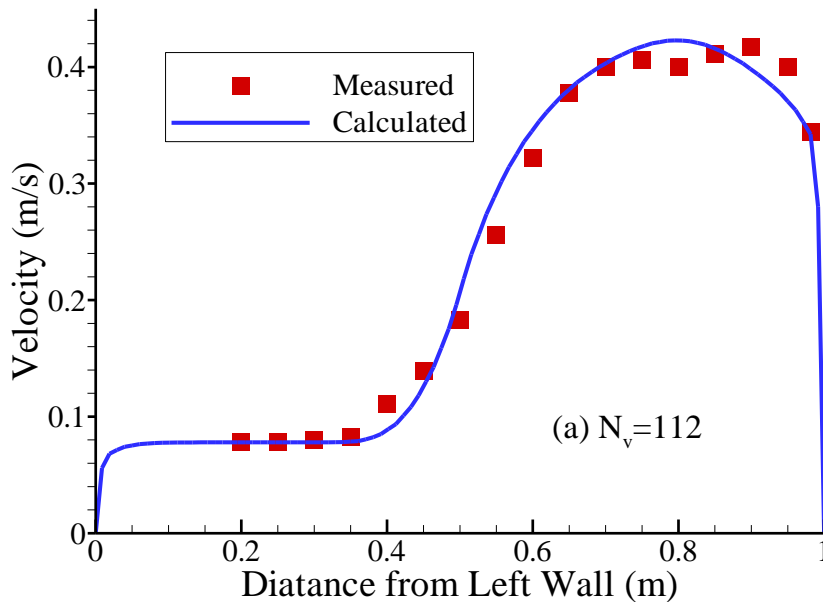
Flow in Compound Channel with Vegetated Floodplain



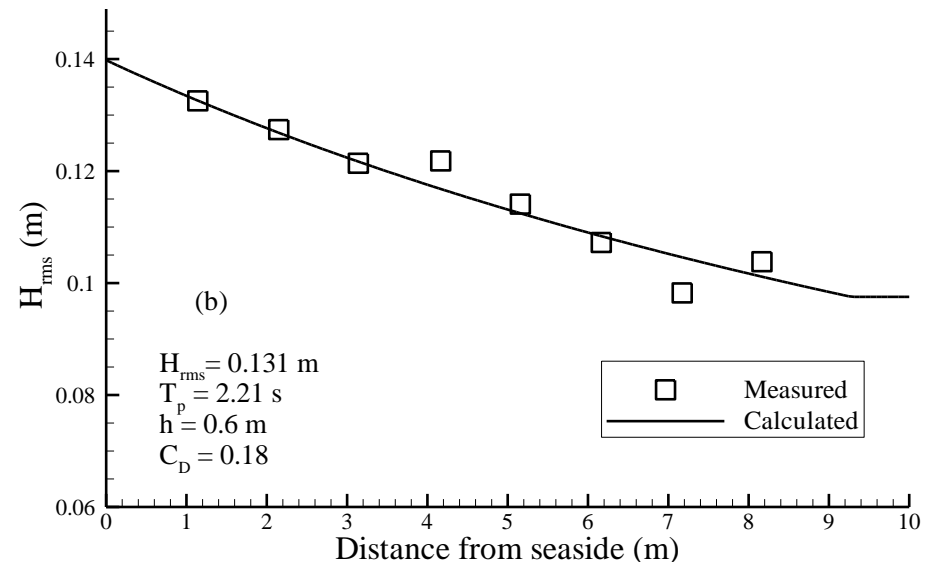
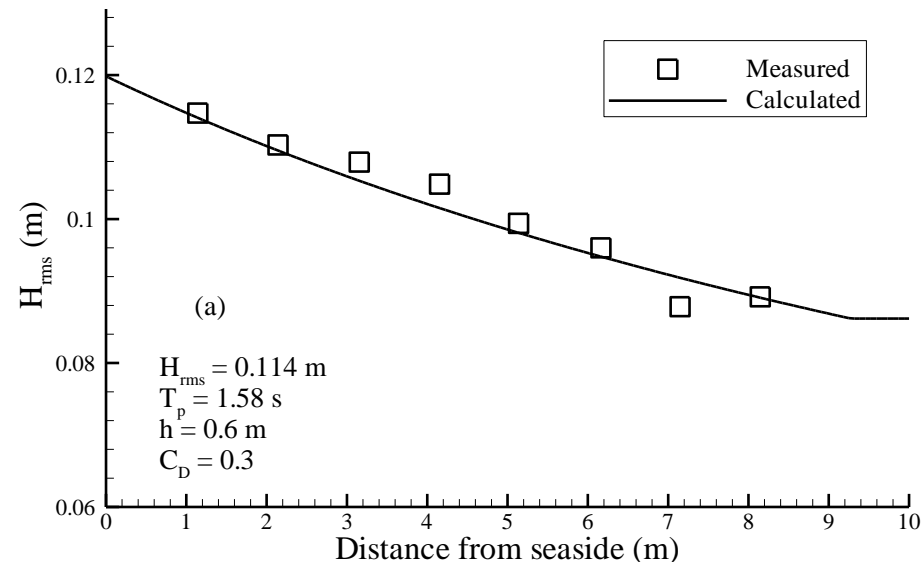
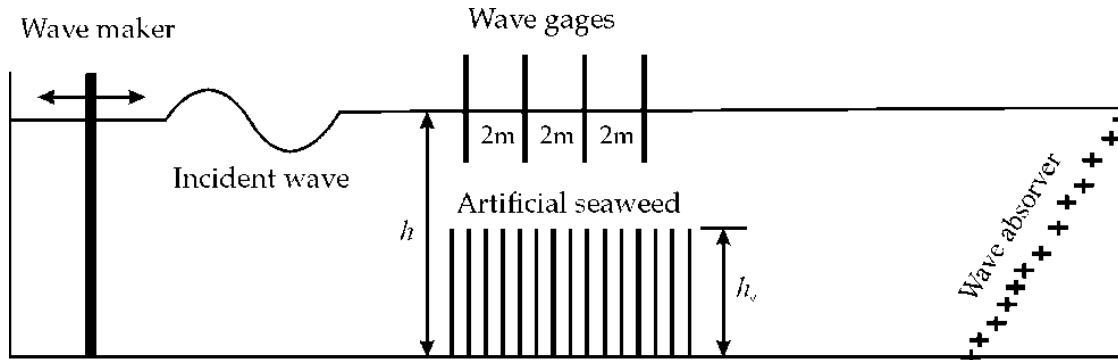
Experiment by Pasche and Rouve (1985)

Vegetation: Rigid wooden rods

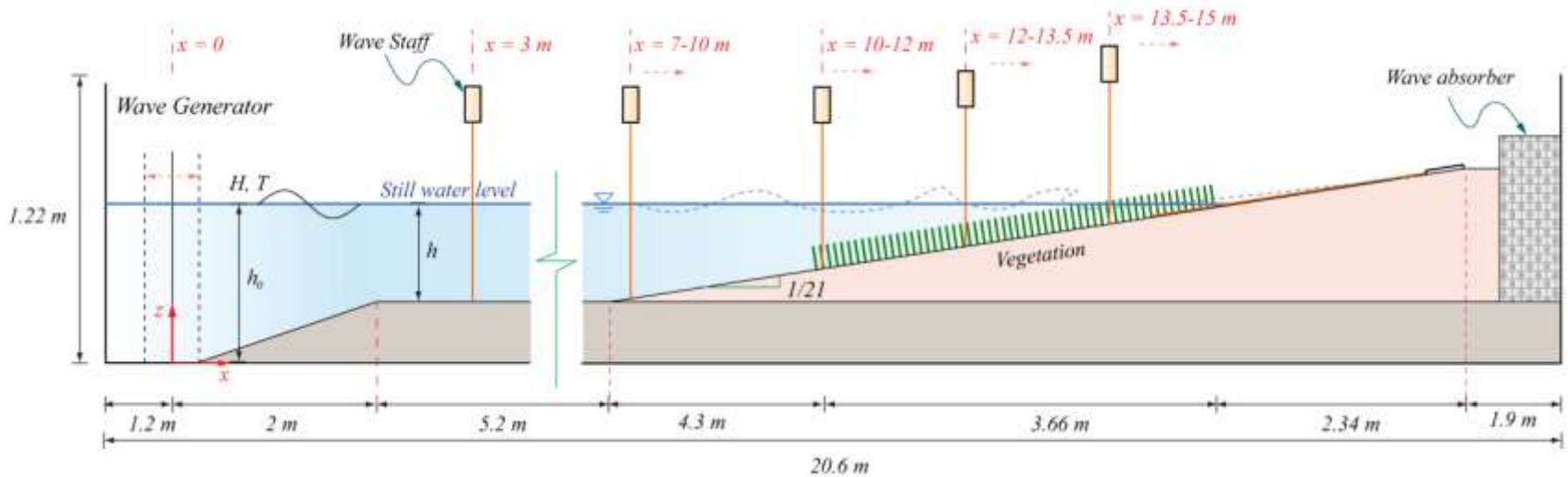
Exp. No.	Discharge (m ³ /s)	Bed slope	Vegetation type	N_v (1/m ²)	Vegetation diameter (m)	C_D
1	0.0365	0.001	Rigid	112	0.012	0.45
2	0.0345	0.0005	Rigid	224	0.012	0.55

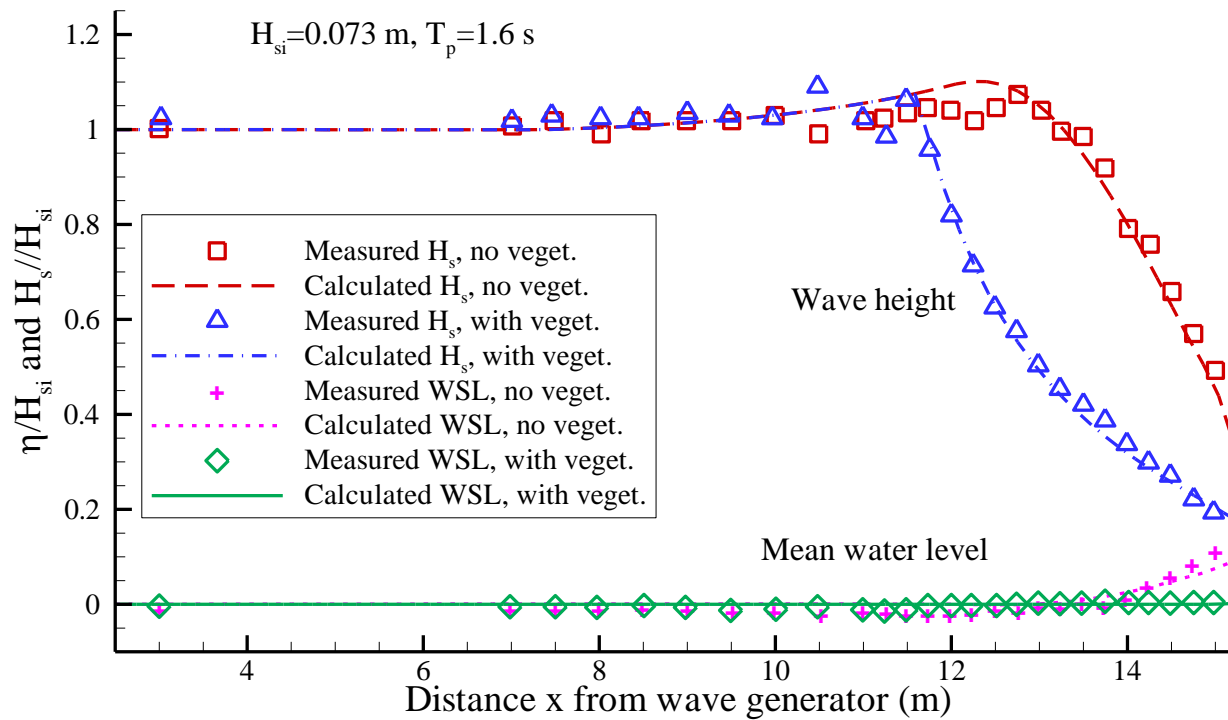
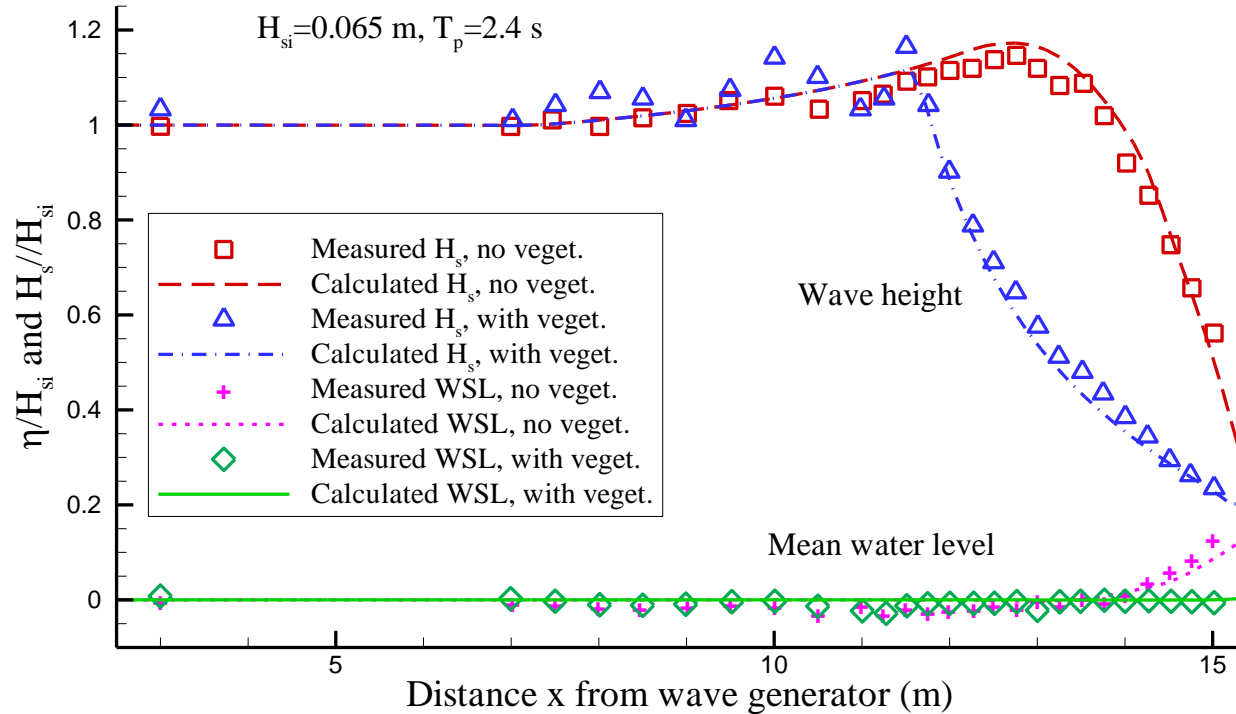


Random Waves through Vegetated Flume



Side View of Wave Runup





Summary

- Effects of vegetation have been extensively investigated by field and lab experiments and numerical modeling.
- A large set of data have been collected and used to analyze the vegetation drag coefficient and wave energy dissipation.
- A series of numerical models have been developed to quantify the wave and surge reduction.
- The models have been tested using a number of laboratory experiments.
- The drag and inertia forces of vegetation are included in the 2D/3D momentum equations and the wave energy loss due to vegetation resistance is in the wave-action balance equation.
- The interaction between currents and waves is considered through a correction factor in the wave dissipation rate.

W. Wu, Y. Ozeren, D. Wren, Q. Chen, G. Zhang, M. Holland, Y. Ding, S.N. Kuiry, M. Zhang, R. Jadhav, J. Chatagnier, Y. Chen, and L. Gordji (2011). Investigation of surge and wave reduction by vegetation, Phase I Report for SERRI Project No. 80037, The University of Mississippi, MS, p. 315, with p. 465 Appendices.

W. Wu, Y. Ozeren, D. Wren, Q. Chen, G. Zhang, M. Holland, R. Marsooli, Q. Lin, R. Jadhav, K.R. Parker, H. Pant, J. Bouanchaud, and Y. Chen (2012). Investigation of surge and wave reduction by vegetation (Phase II) —Interaction of Hydrodynamics, Vegetation and Soil, Phase II Report for SERRI Project No. 80037, The University of Mississippi, MS, p. 395.

W. Wu and R. Marsooli (2012). “A depth-averaged 2-D shallow water model for breaking and non-breaking long waves affected by rigid vegetation.” *Journal of Hydraulic Research, IAHR*, 50(6), 558–575.

W. Wu, M. Zhang, Y. Ozeren, and D. Wren (2013). “Analysis of vegetation effect on waves using a vertical 2-D RANS model.” *Journal of Coastal Research*, 29(2), 383–397.

W. Wu (2014). “A 3-D phase-averaged model for shallow water flow with waves in vegetated water.” *Ocean Dynamics*, 64(7), 1061-1071.

R. Marsooli and W. Wu (2014). “Numerical investigation of wave attenuation by vegetation using a 3D RANS model.” *Advances in Water Resources*, Accepted for publication.

Y. Ozeren, D. Wren, and W. Wu (2014). “Experimental investigation of wave attenuation through model and live vegetation.” *Journal of Waterway, Port, Coastal, and Ocean Engineering (ASCE)*, published online, DOI: 10.1061/(ASCE)WW.1943-5460.0000251.